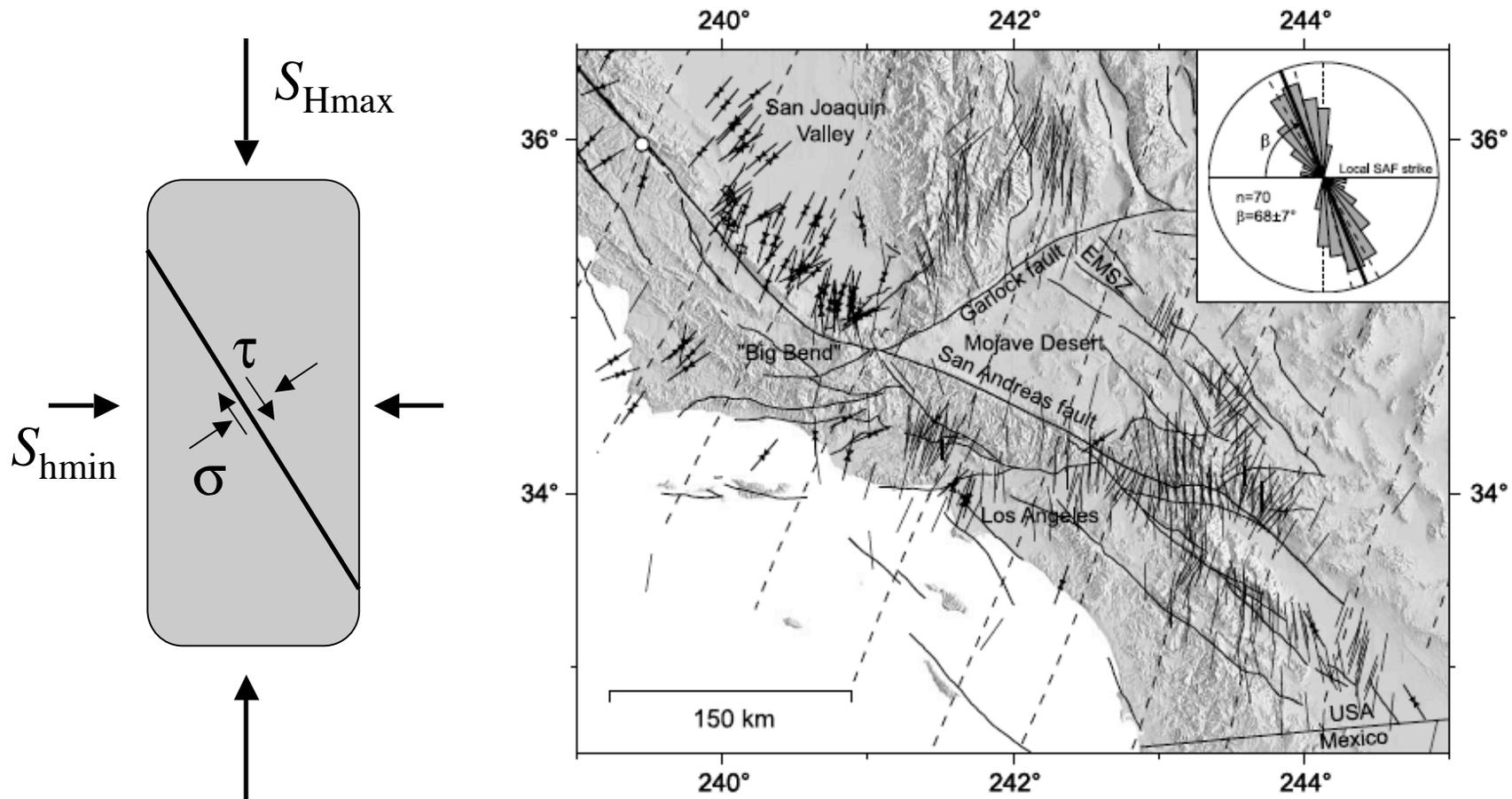


# Earthquake Ruptures with Thermal Weakening and the Operation of Faults at Low Overall Stress Levels

Eric M. Dunham (Harvard), Hiro Noda (Caltech), James R. Rice (Harvard)

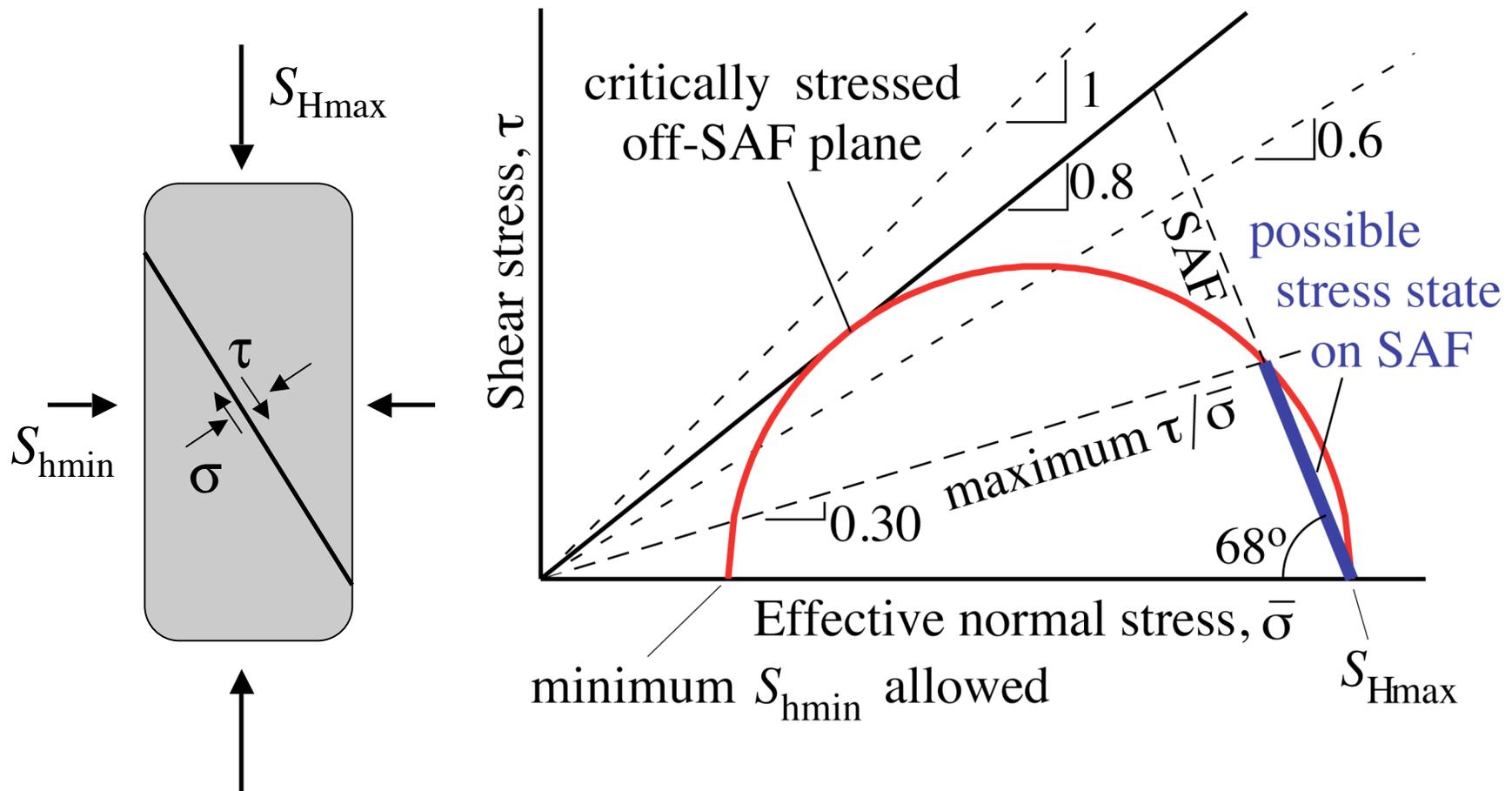
Maximum compressive stress at  $68 \pm 7^\circ$  from local SAF strike  
(from borehole breakouts, hydraulic fracturing, earthquake focal mechanisms)



[Townend and Zoback, 2004]

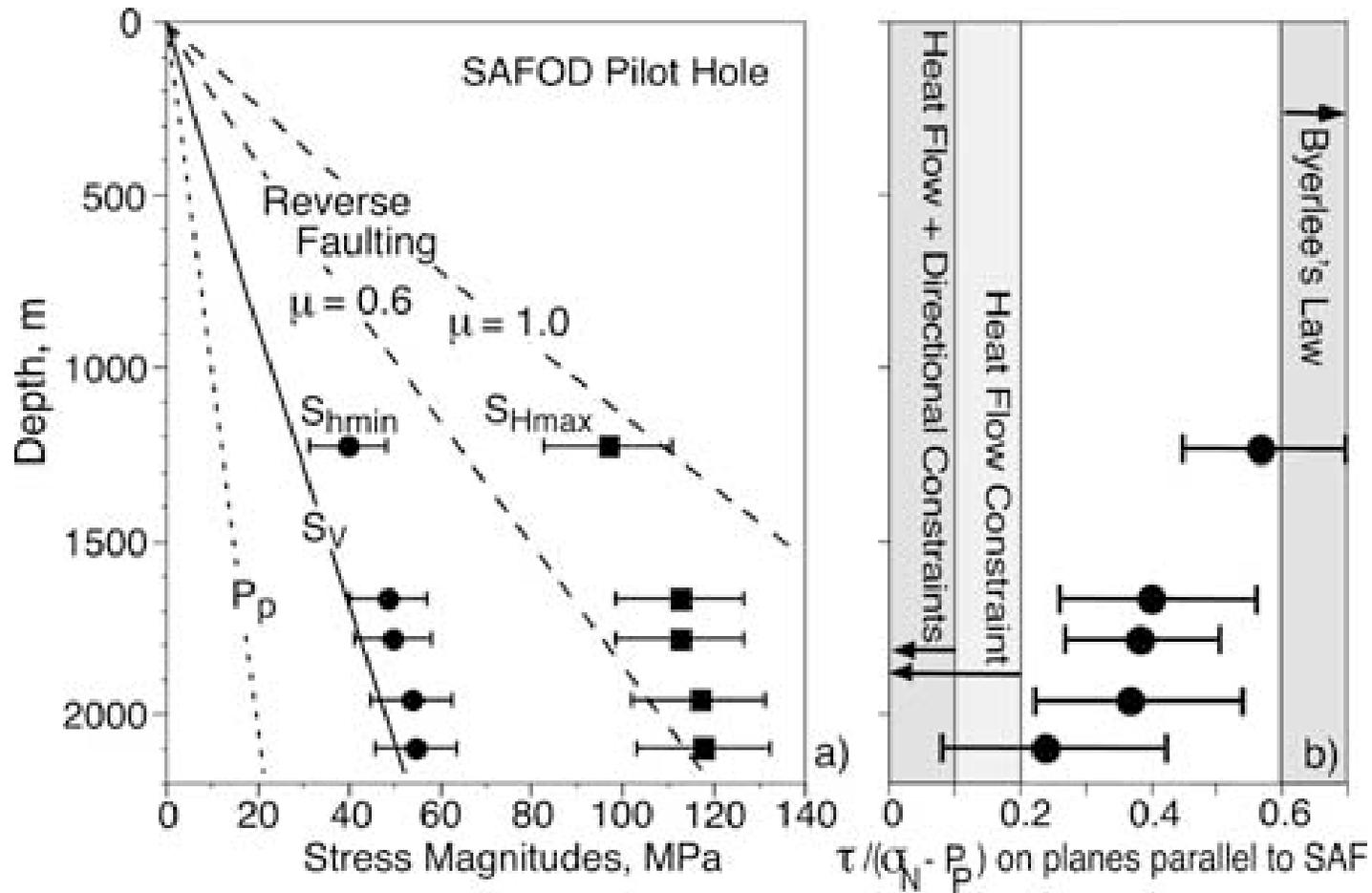
1. Maximum compressive stress at  $68 \pm 7^\circ$  from local SAF strike
2. Stresses in crust cannot exceed static friction (assuming  $f_s \sim 0.8$ )

$\Rightarrow$  Maximum  $\tau/(\sigma-p)$  on SAF is  $\sim 0.3$



[Noda, Dunham, and Rice, submitted 2008]

# Stresses in SAFOD Pilot Hole: $\tau/(\sigma - p) \approx 0.2 - 0.3$ at 2.2 km depth



[Hickman and Zoback, 2004]

# Fault Mechanics and Dynamic Weakening Mechanisms

**Stress constraints:** low stresses acting on major faults

**Geologic constraints:** lack of pseudotachylytes (melted rock) near slip surface

**Heat flow constraints:** lack of heat flow signature around faults

Dynamic weakening reduces fault shear strength,  $\tau$ , but *only during rapid sliding* ( $V \sim \text{m/s}$ ); caused by changes in:

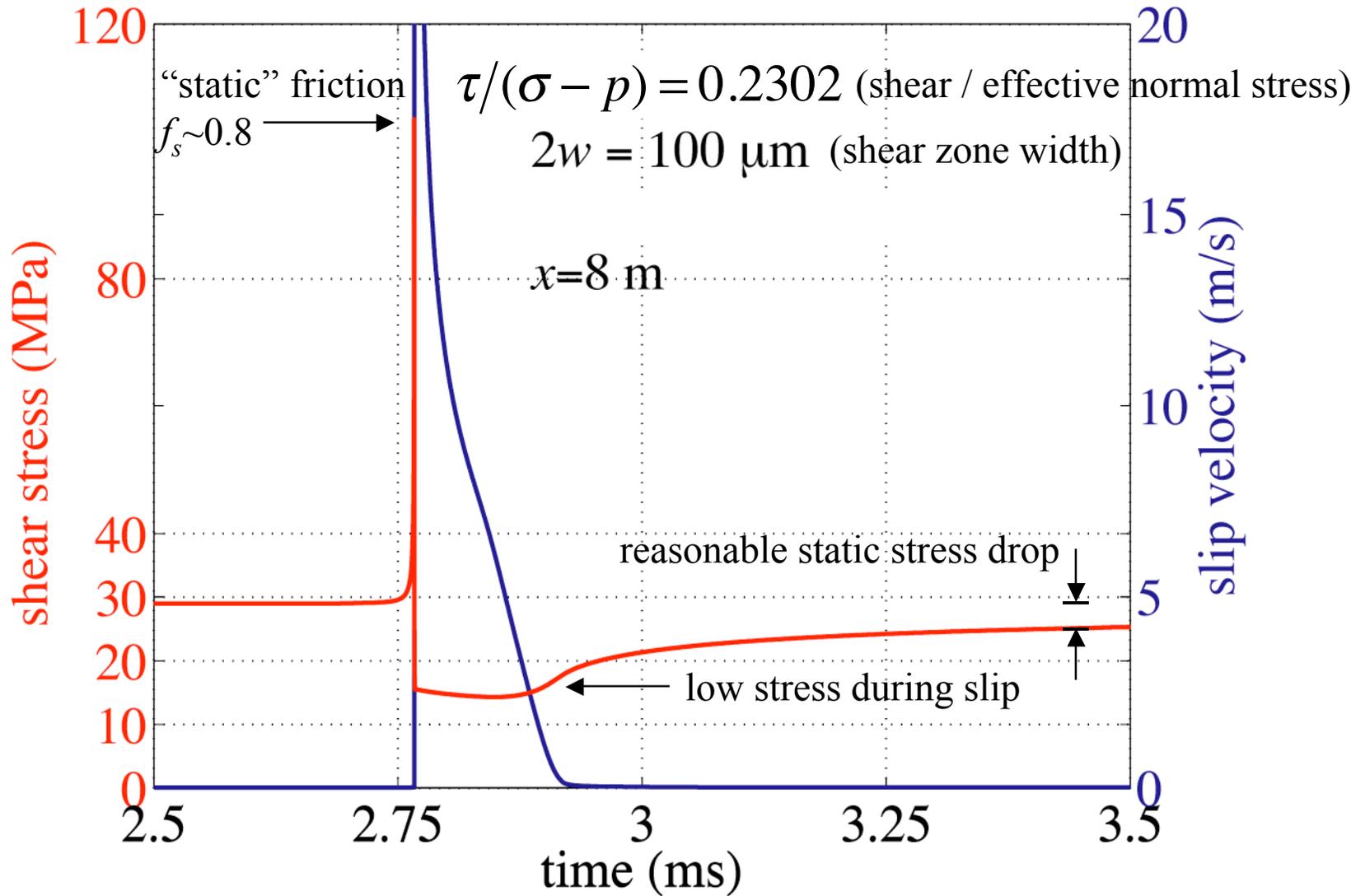
$$\tau = f(\sigma - p)$$

$f$  = coefficient of friction (reduced by flash heating of asperity contacts)

$p$  = pore pressure (raised by thermal pressurization)

$\sigma$  = normal stress

# Features of a Dynamic Weakening Model

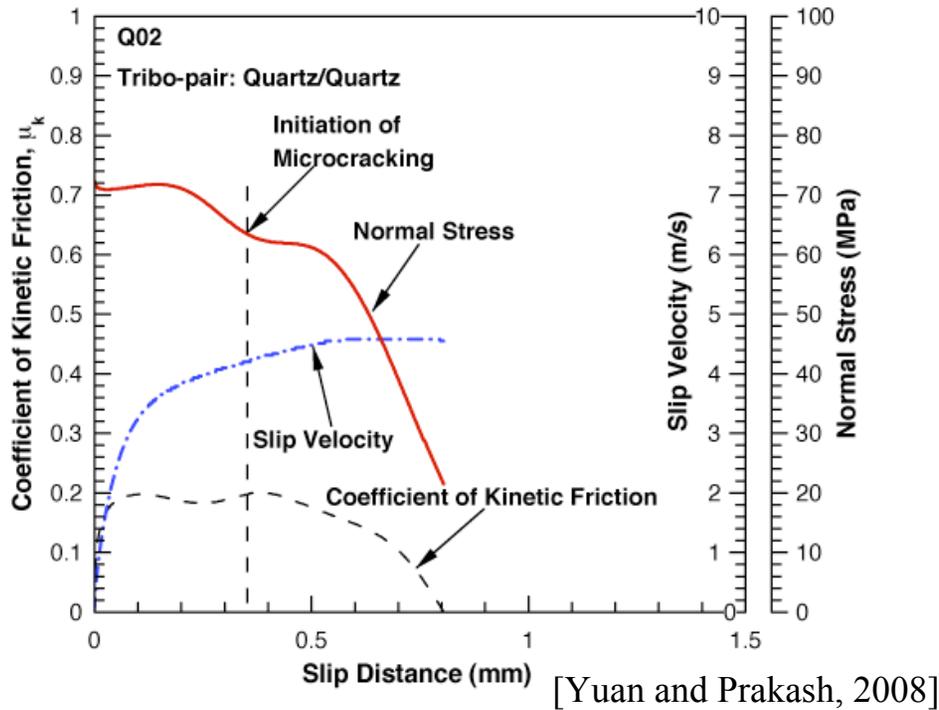


[Noda, Dunham, and Rice, submitted 2008]

# Weakening Mechanisms

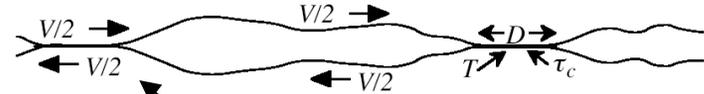
## 1. Flash Heating of Microscopic Asperity Contacts

*Strongly velocity-weakening friction*



(in rate-and-state framework, using lab values of  $L \sim 10 \mu\text{m}$ )

$$\frac{df}{dt} = \frac{a}{V} \frac{dV}{dt} - \frac{V}{L} [f - f_{ss}(V)]$$



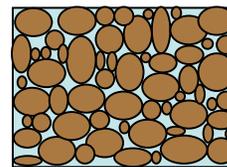
contacts heated until they weaken/melt (or slide out of existence)

[Rice, 1999, 2006; Beeler and Tullis, 2003; Tullis and Goldsby, 2003; Beeler et al., 2008]

## 2. Thermal Pressurization of Pore Fluid

Conservation of energy and fluid with

- distributed shear zone ( $\sim 100 \mu\text{m}$  wide)
- diffusion of heat and fluid (“adiabatic, undrained” when transport neglected)
- thermal and hydraulic properties from drilling projects and exhumed faults



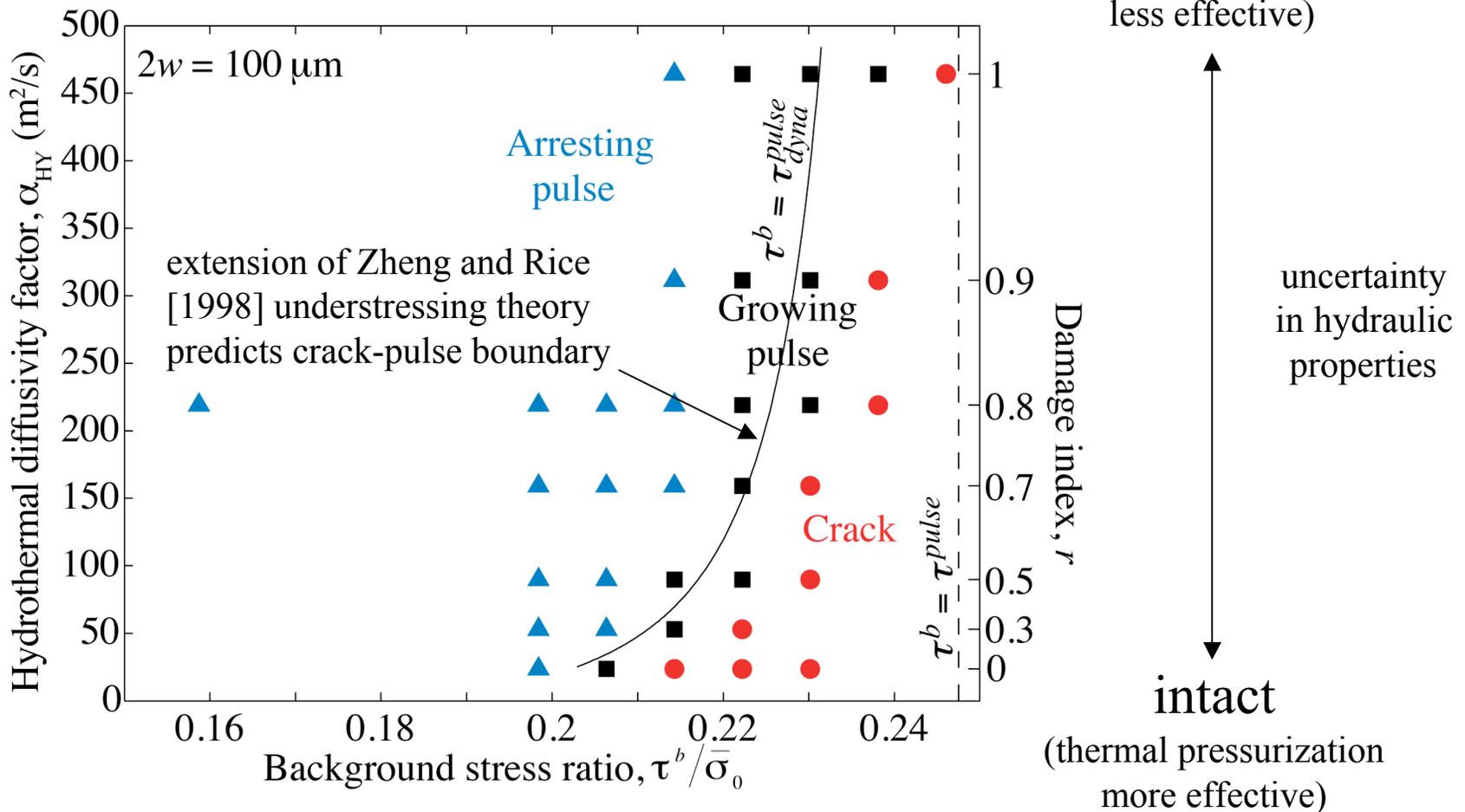
undrained pressurization

$$\left( \frac{\partial p}{\partial T} \right)_u \sim \text{MPa/K}$$

[Rice, 2006; building on Sibson, 1973 and many others]

# Faults Host Ruptures at Low Background Stress Levels

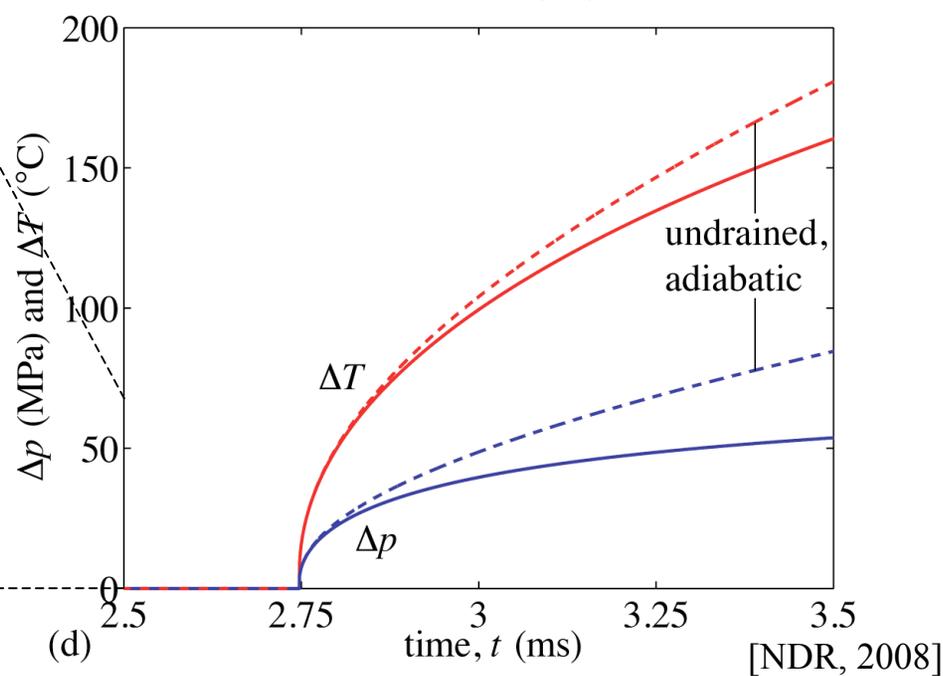
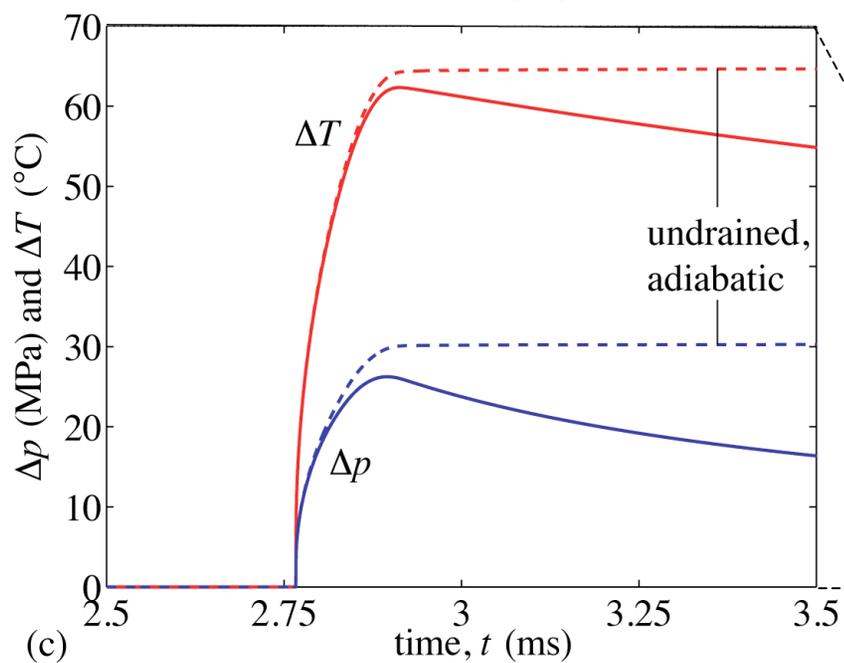
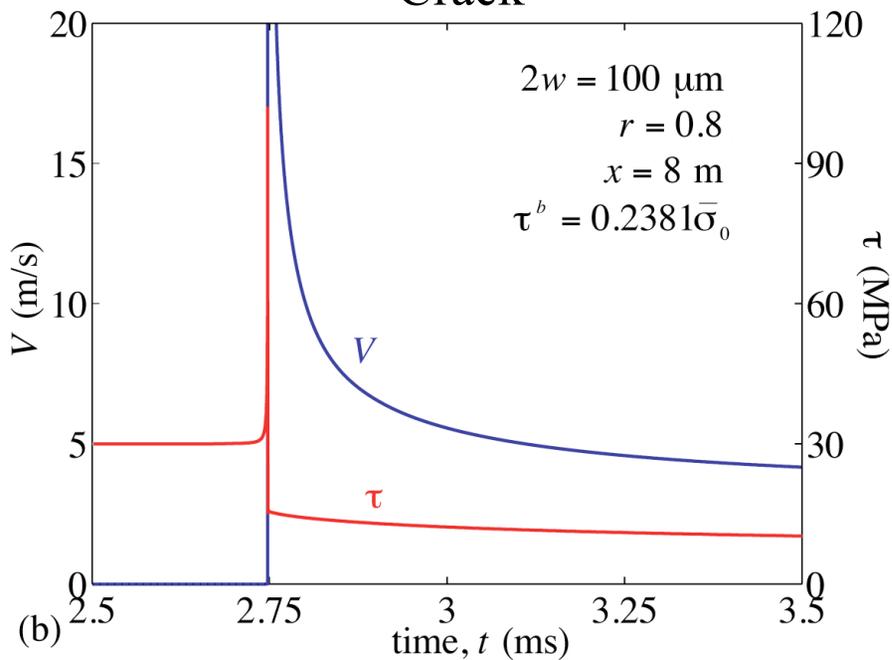
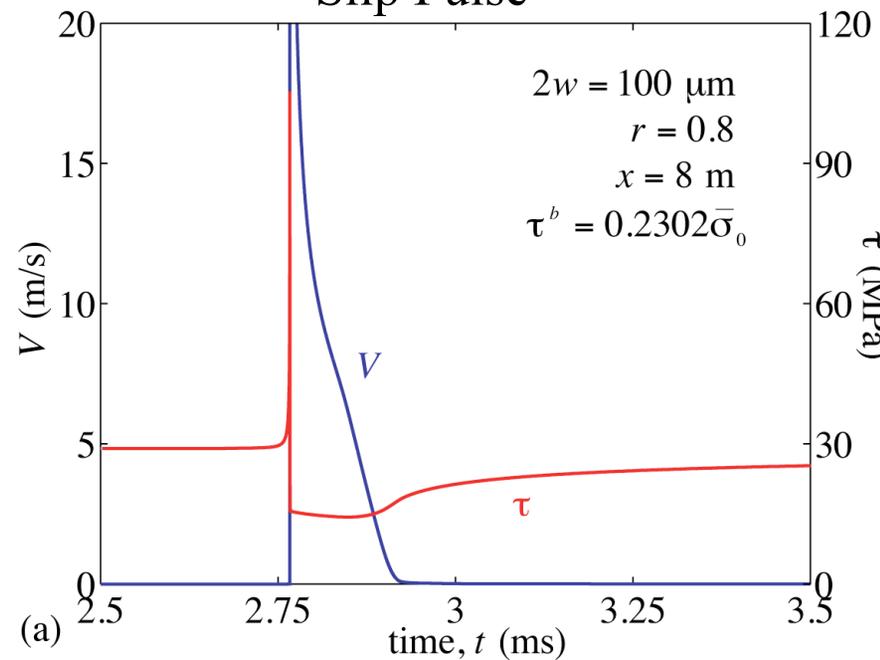
(flash heating is essential,  
thermal pressurization plays minor role)



[Noda, Dunham, and Rice, submitted 2008]

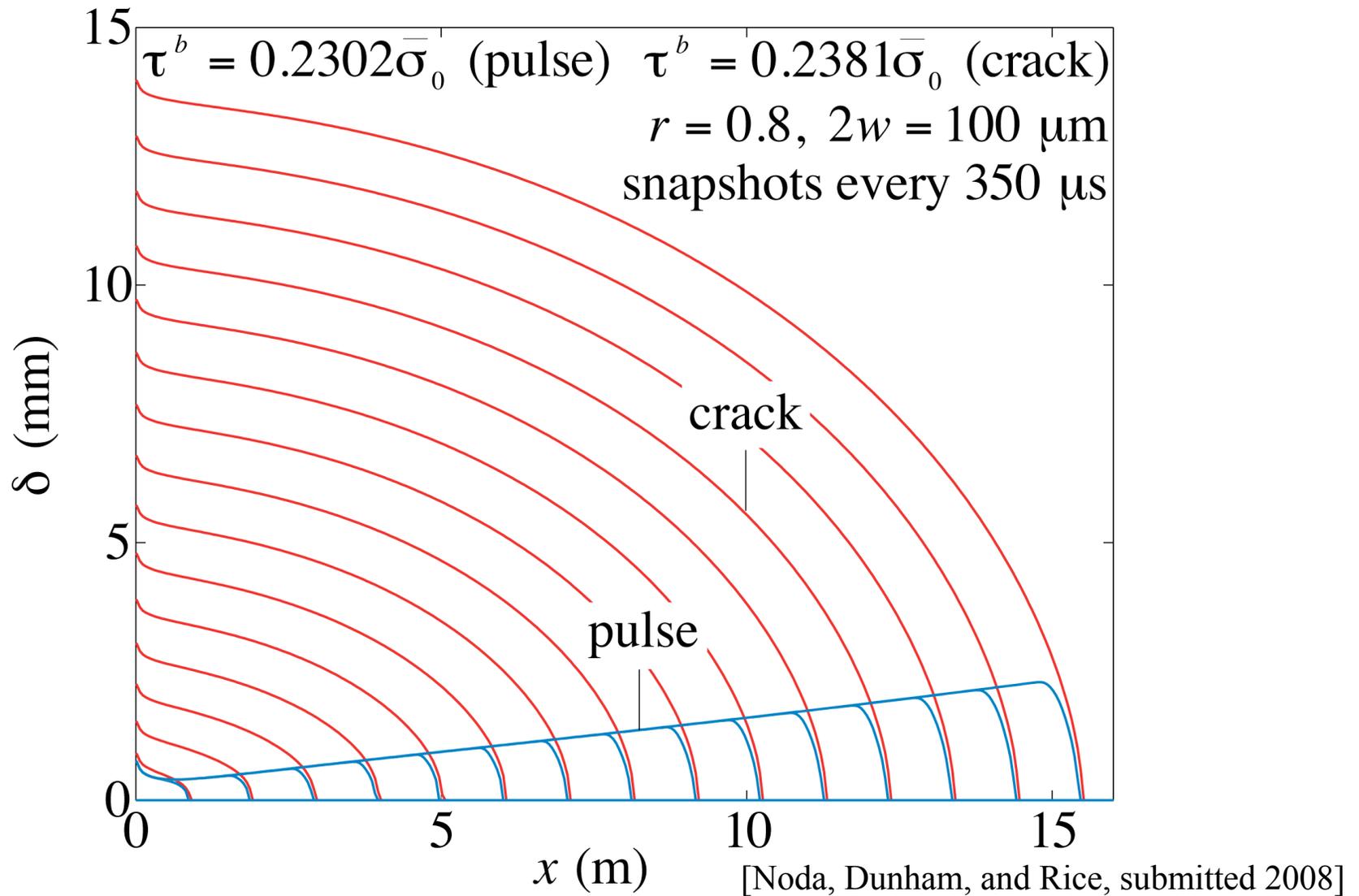
### Slip Pulse

### Crack

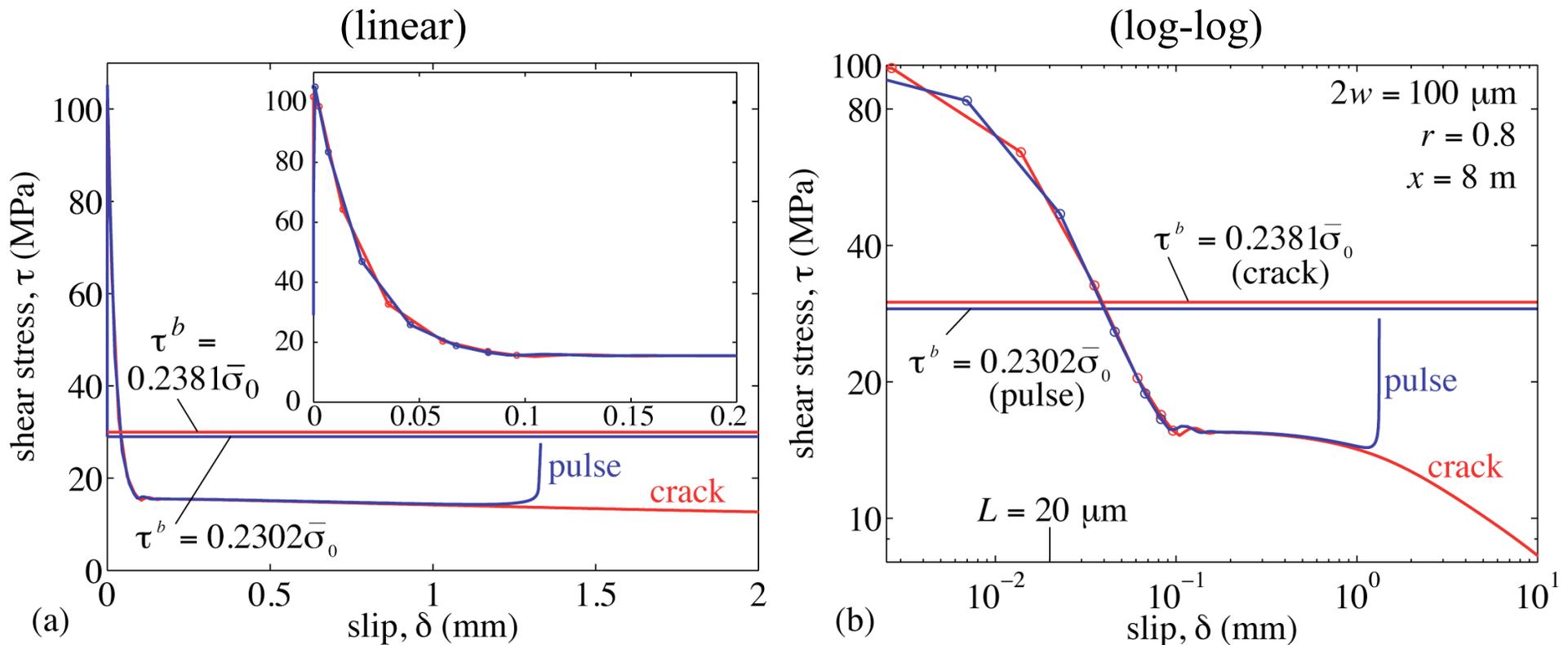


# Self-Similar Scaling

Scaling (of slip pulses, not cracks) consistent with natural earthquakes:  
~0.14 mm slip / m rupture length = 0.14 m/km



# Succession of Weakening Mechanisms at Rupture Front



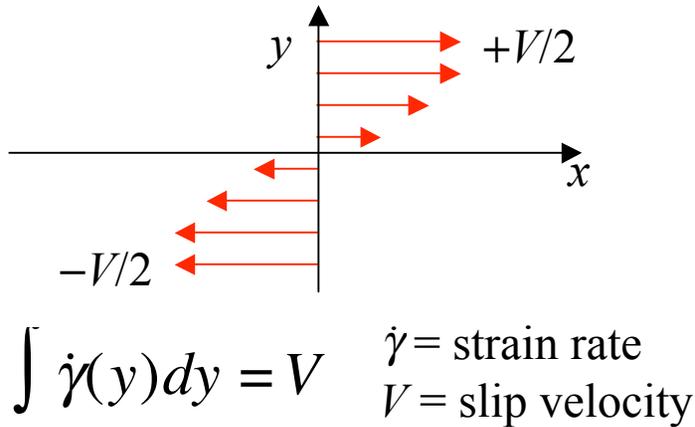
State evolves very quickly, subsequent weakening from thermal pressurization

Summary: Strong rate-weakening permits slip pulses on faults at  $\tau/(\sigma-p) \sim 0.3$  (rupture mode fairly insensitive to thermal pressurization)

Open question: How to use these laws in large-scale simulations? Increase  $L$ ? Increase both  $L$  and hydraulic properties (holding dimensionless ratios fixed)?

[Noda, Dunham, and Rice, submitted 2008]

# Thermal Pressurization of Pore Fluids by Distributed Shear Heating



## Conservation of energy

$$\frac{\partial T}{\partial t} = \cancel{\alpha_{th} \frac{\partial^2 T}{\partial y^2}}^{\text{adiabatic}} + \frac{\tau \dot{\gamma}}{\rho c}$$

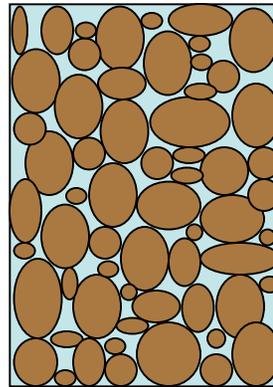
$T$  = temperature  
 $\alpha_{th}$  = thermal diffusivity  
 $\rho c$  = volumetric heat capacity

## Conservation of fluid mass (neglecting changes in $p$ from fault-zone strains)

$$\frac{\partial p}{\partial t} = \cancel{\alpha_{hy} \frac{\partial^2 p}{\partial y^2}}^{\text{undrained}} + \Lambda \frac{\partial T}{\partial t}$$

$p$  = pore pressure  
 $\alpha_{hy}$  = hydraulic diffusivity  
 $\Lambda$  = undrained pressurization

heat while holding fluid mass  $m$  fixed (undrained response)



- thermal expansion coefficient of water ( $\sim 10^{-3} \text{ K}^{-1}$ )  $\gg$  solid matrix
- water and matrix equally compressible ( $\sim \text{GPa}^{-1}$ )

$$\Lambda = \left( \frac{\partial p}{\partial T} \right)_m \sim \text{MPa/K}$$

[Rice, 2006; building on Sibson, 1973 and many others; thermal and hydraulic properties of fault-zone materials constrained by measurements from exhumed faults and drilling projects)]