

Antenna Design and Site Planning Considerations for MIMO



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A One-Slide MIMO Primer

Generalized Shannon Bound:

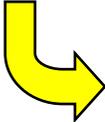
$$C = B \log_2 \det \left[\mathbf{I}_{N_R} + \frac{\Gamma}{N_T} \mathbf{H}\mathbf{H}' \right]$$

Capacity [b/s] Bandwidth [Hz] Matrix of Channel Coefficients [$N_R \times N_T$]
 Mean SNR per RX antenna

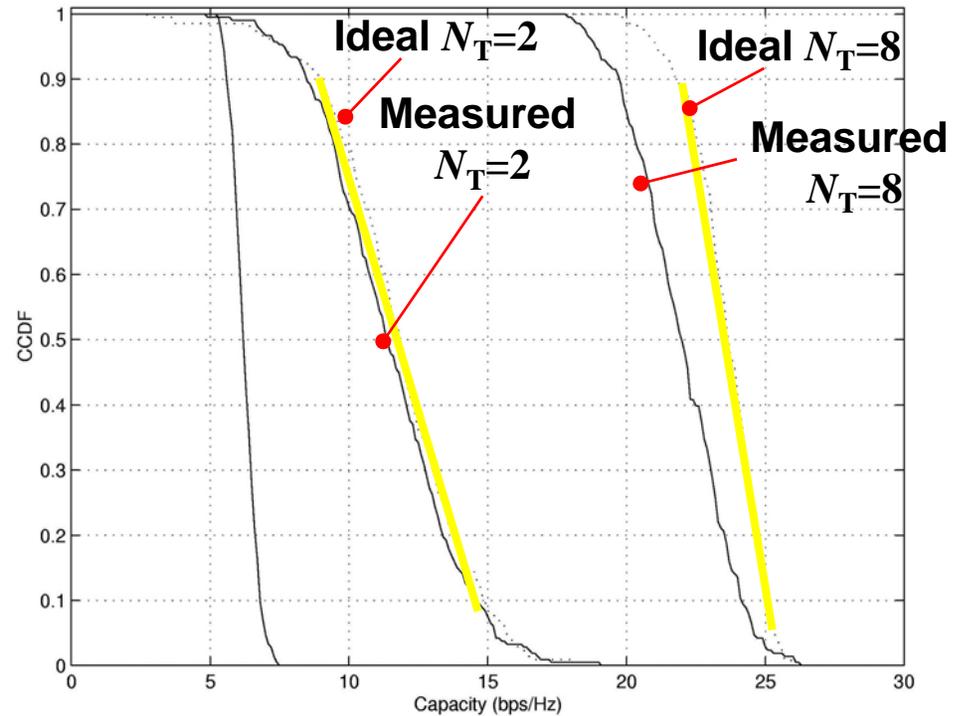
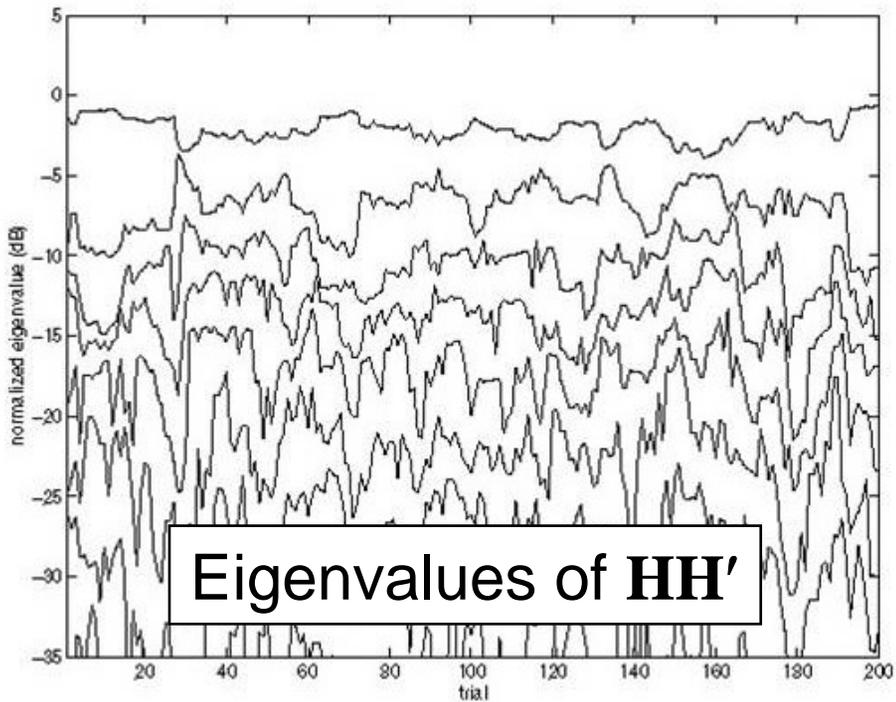
G.J. Foschini and M.J. Gans, "On Limits of Wireless Communications in a Fading Environment when Using Multiple Antennas", *Wireless Personal Communications* (Kluwer), 6:311-335, 1998.

$$N_T=1 \text{ or } N_R=1 \rightarrow \text{rank}\{\mathbf{H}\mathbf{H}'\}=1 \rightarrow C \propto \log_2 N$$

$$N_T>1 \text{ and } N_R>1 \text{ and } \text{rank}\{\mathbf{H}\mathbf{H}'\}>1 \rightarrow C \propto N$$


 Up to $k = \min\{N_T, N_R\}$ independent MIMO "subchannels", each with SNR \propto the associated eigenvalues of $\mathbf{H}\mathbf{H}'$

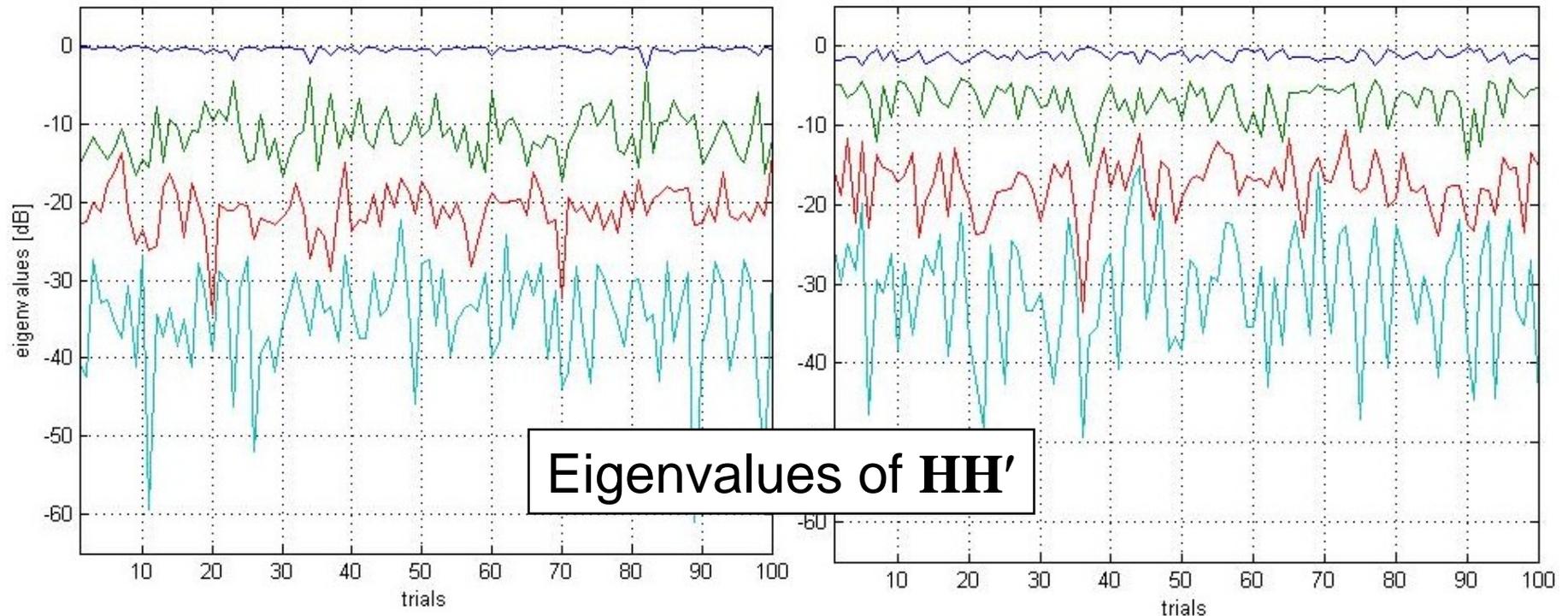
What We Like to See!



- 2.4 GHz
- $N_R=8$

What We Like to See?

- Indoor: Cluttered laboratory, approx 5 m x 10 m
- About 2 meters between arrays
- Transmit Array: 4 $\lambda/4$ monopoles, V-pol, 0.25λ spacing
- Receive Array: *same*

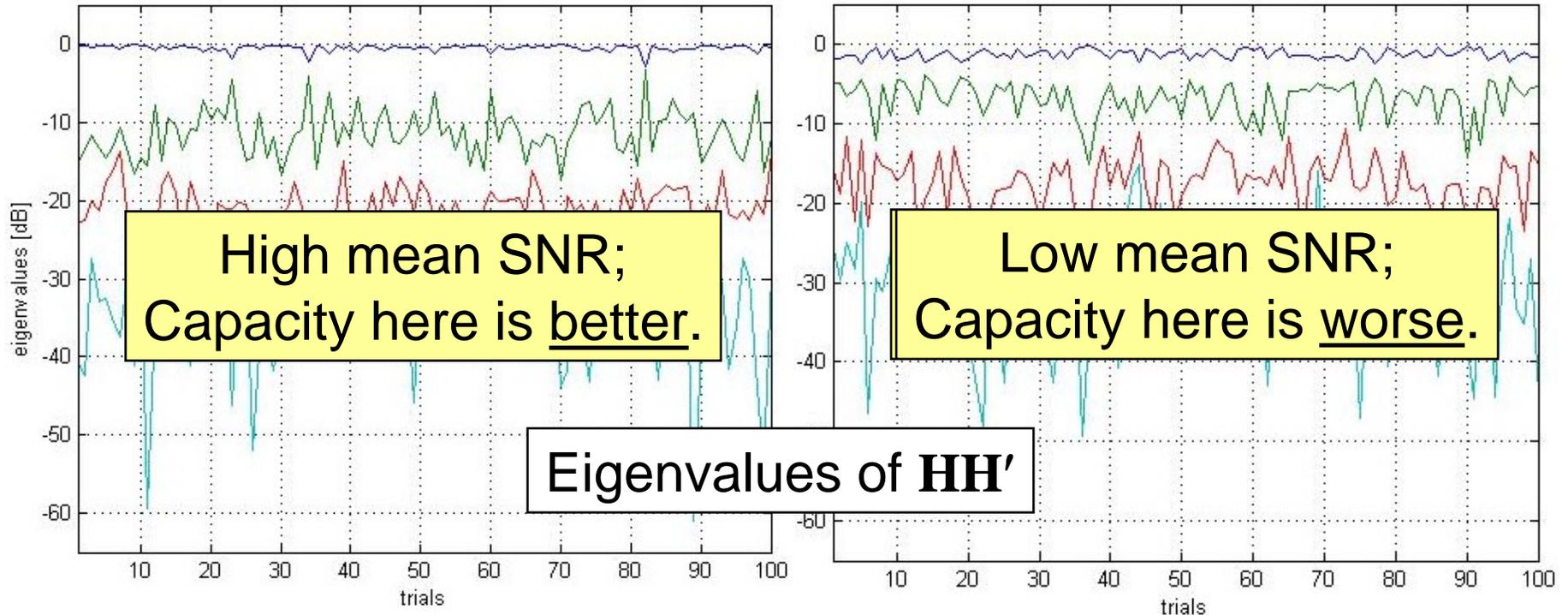


4 x 4: Optical LOS Exists

4 x 4: Optical LOS Blocked
using 1 m x 2 m metal plate

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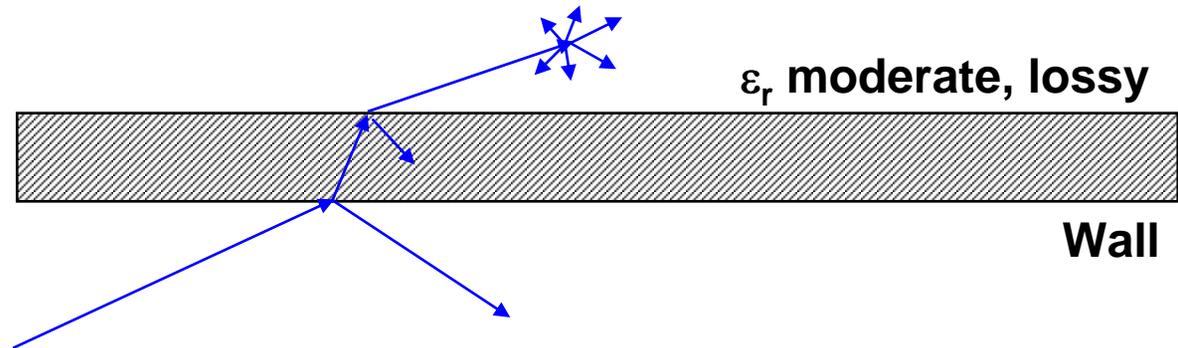
Antenna Array Design for MIMO

- [CNR: “SNR averaged over a period \gg coherence time”]
- A well-designed MIMO antenna system should:
 - Achieve size and cost goals (constrains N_T and N_R)
 - Achieve the required CNR over the coverage area
 - Maximize the diversity order
 - Maximize the “effective rank” k_e (i.e., the number of accessible MIMO subchannels with “useable” CNR)
- Some dimensions of this optimization:
 - Number, type, and polarization of antenna elements
 - Element spacing and geometry
 - Location and orientation of arrays within rooms and hallways
- Really two problems:
 - How to design arrays that perform OK anywhere (the “Circuit City” problem)
 - How to design & place arrays for specific sites
- This talk is really about the latter, but has implications for the former

Indoor Propagation Characteristics

Horizontal Plane:

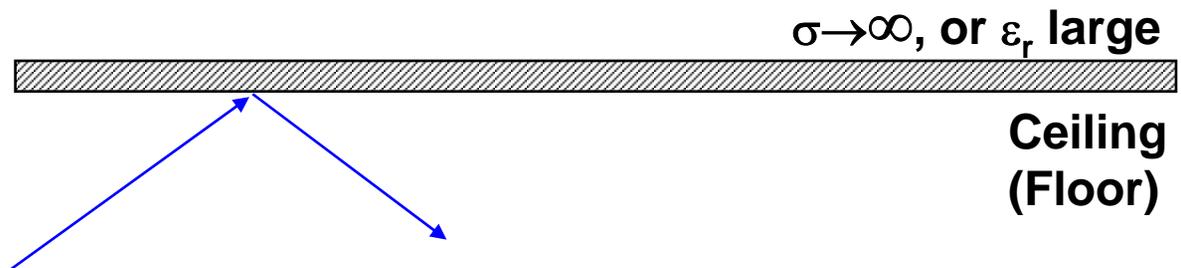
- Copious scattering,
- Leakage,
- Loss



Vertical Plane:

- Some coherent scattering
- Efficient Containment

(Most office buildings)



Indoor Propagation Consequences

- **Rooms:**
 - Angle spread (AS) is large → Exploitable space diversity
 - High xpol; no pol. preference → Exploitable pol. diversity
- **Hallways:**
 - AS is narrower
 - Confined in elevation plane by floor and ceiling
 - Dominated in azimuth plane by coherent scattering
 - Lower xpol compared to rooms → pol. diversity often not available
- **Delay spread usually small compared to inverse bandwidth**
 - Usually flat fading only, so:
 - Spatial diversity is very important

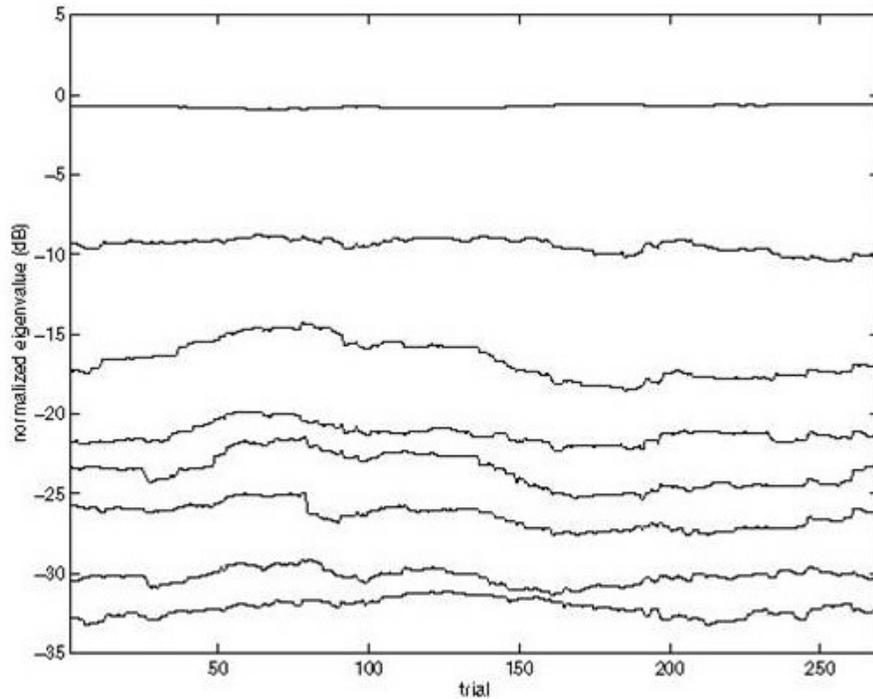
Element Pattern and Polarization

- **Element pattern:**
 - Usually preferred to match this to the AS to intercept all available power
 - Rooms: Low gain elements for sure
 - Hallways: Low gain elements usually OK since poor match to angle spread is usually offset by reduced path loss
- **Polarization:**
 - Match to dominant polarization to maximize CNR
 - In rooms, received signals are only weakly polarized, so polarization diversity can be an effective option
 - In hallways, received signals tend to be strongly polarized, so polarization diversity is often not effective (thus using it squanders CNR). Better to match to the dominant polarization.
- These guidelines apply equally to MIMO arrays.

Diversity vs. Beamforming vs. MIMO

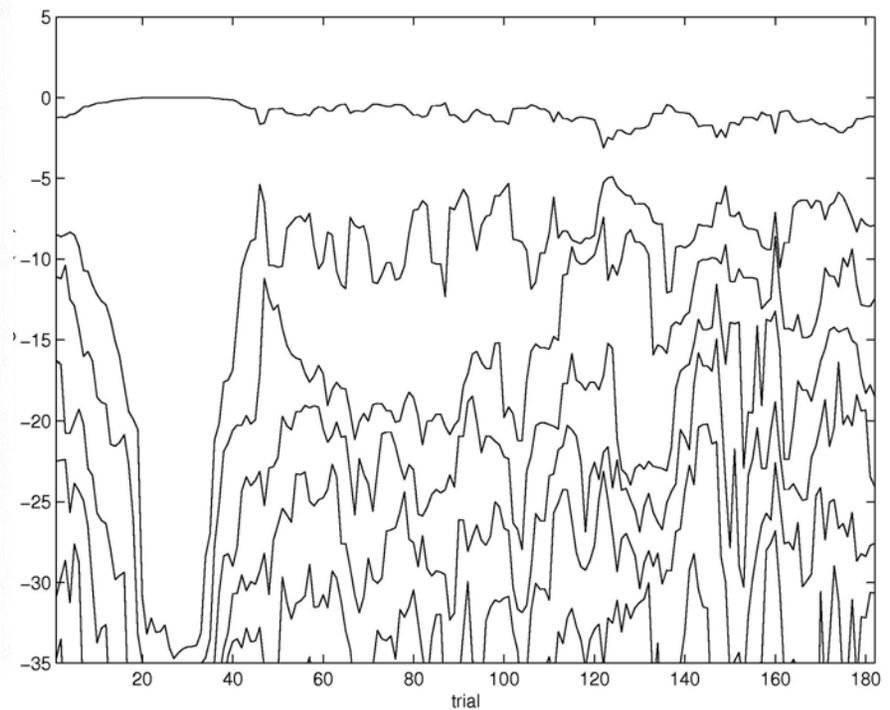
- **Nothing works unless the CNR is sufficiently large...so that is the first priority.**
- **When CNR is reasonable, the ability to maximally exploit (rank=1) diversity is important, since the indoor channel is almost always limited by flat fading. This will be good for MIMO as well.**
- **When the CNR is low, the ability to make directional patterns, or form beam(s), to improve CNR is important (in this case, might as well make array “compact” with spacings $< 0.7\lambda$)**
- **Then, consider ability to access MIMO subchannels...**

Real-World MIMO Can Be Quirky



**Persistent (minutes...)
Near-Keyhole Condition
*Poor CNR conditions***

Capacity: LOW



**Transient (seconds...)
“Hard” Keyhole Condition
*High CNR conditions***

Capacity: HIGH

- So, the actual rank of the channel may not mean much.
- Also, SNR normalization can yield very misleading results!

Optimizing for Large AS (Rooms)

- “Environmental” spatial autocorrelation $\rho \sim J_0(2\pi d/\lambda)$ requires d on the order of λ to be significantly decorrelated
- This is in fact the case for arrays of low gain elements when $d > 2\lambda$ or so
- For d on the order of $A_e^{1/2}$ (0.36λ for a resonant dipole) or less, mutual coupling becomes dominant:
 - Coupling modifies element impedance \rightarrow degrades match WRT a standard impedance \rightarrow degrades radiation efficiency \rightarrow CNR suffers
 - Coupling alters element patterns (pattern diversity...?), but:
 - Studies that address both issues show that poor radiation efficiency tends to dominate for $d < A_e^{1/2}$.
- So for large AS (and in general...):
 - Linear arrays with spacings $> \lambda$ or are preferred
 - Arrays with spacings down to $\sim A_e^{1/2}$ are useable
 - Arrays with spacings less than this require EM-savvy design and matching networks to stave off CNR degradation

How Close Can Two Parallel Dipoles Be?

d	$ \rho $	$d / A_e^{1/2}$	$ Z_{12} / Z_1 $	Remarks
$>\lambda$	$<.3$	>2.7	<0.3	Tend to be limited only by environmental correlation
$\lambda/2$	$\sim.3$	1.4	(0.1)	Onset of “significant” MC effects
$\lambda/3$	($\sim.2$)	0.9	0.4	Tailored Impedance matching becomes important for reasonable SNR; Pattern diversity becomes useable
$\lambda/4$	$\sim.5$	0.7	0.7	Mutual coupling directly degrades correlation
$\lambda/10$	$\sim.9$	0.3	0.9	Practical limit of impedance matching AND channel-provided decorrelation

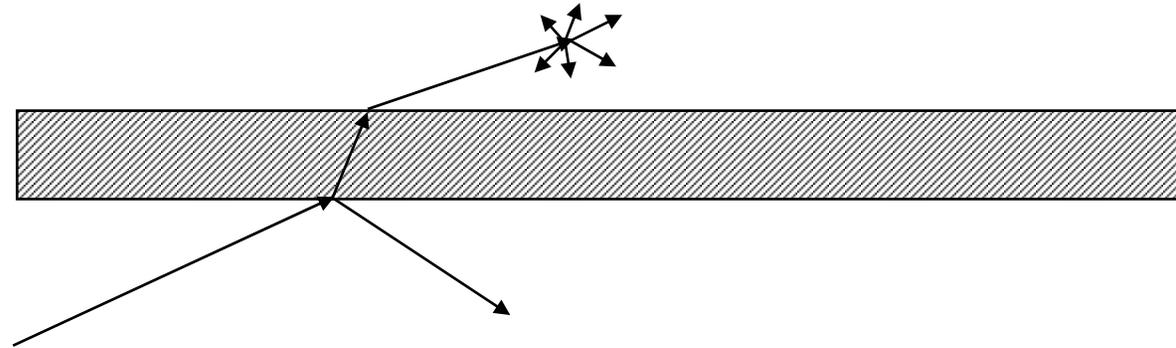
Optimizing for Small AS (Hallways)

- **Greater spacings now required to achieve the same level of diversity, so it is now easy to be dominated by this issue as opposed to mutual coupling**
- **Rule of thumb: $d/\lambda > 60^\circ/AS$ lambda required for significant decorrelation** (Diversity requires a “beamwidth” that is narrow enough to resolve multipath clusters)
- **Geometry should be linear and perpendicular to mean angle of arrival**
- **It is often impossible to achieve significant diversity in available aperture due to space limitations**
 - **In this case consider directional elements or beamforming** (recall, defined here as maximizing the CNR, not the SNR)

How Hallways Can be a Headache (1)

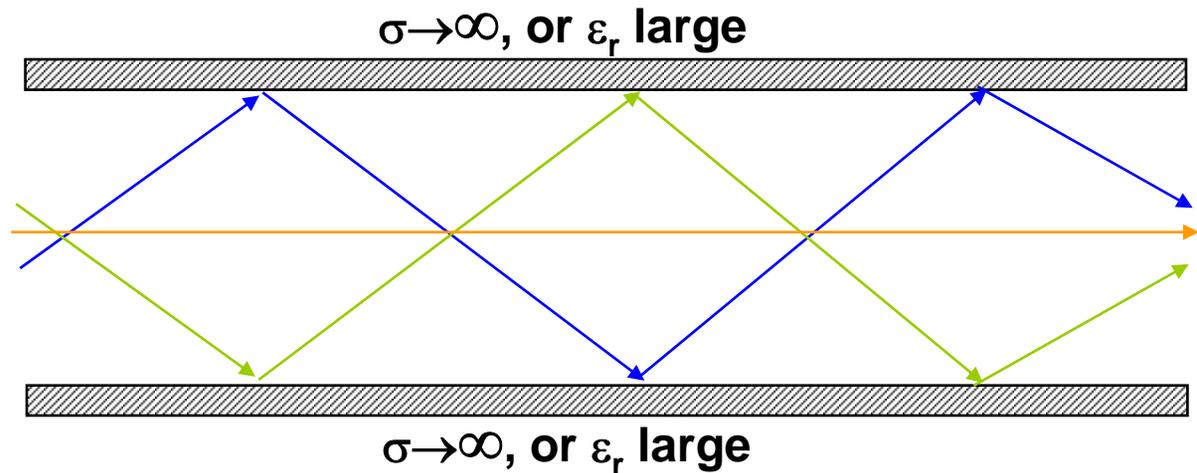
Horizontal Plane:

- Leakage into rooms,
- Incoherent scattering,
- Loss

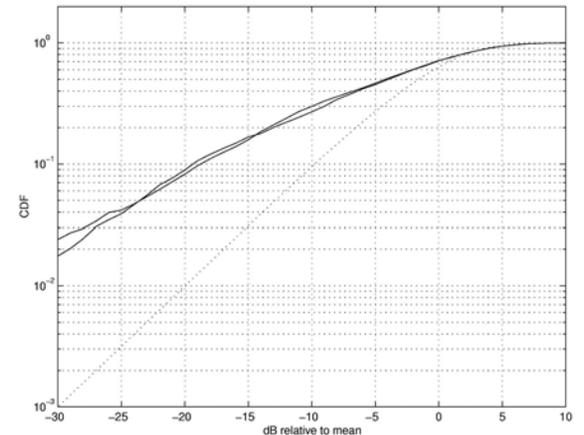
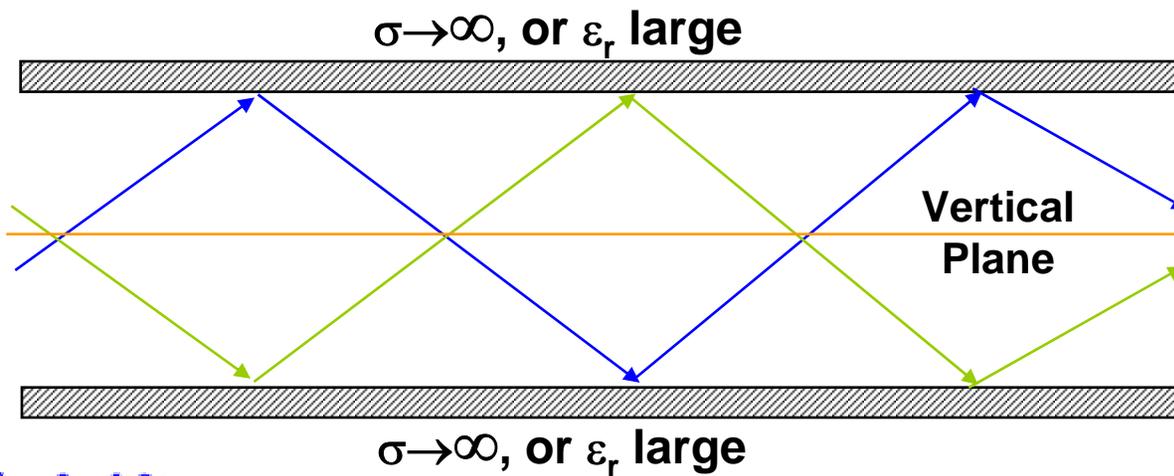
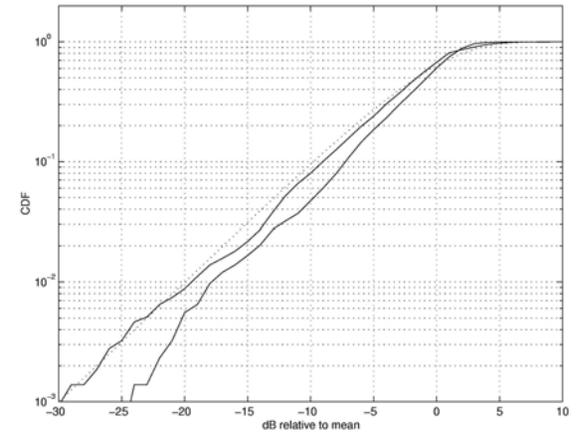
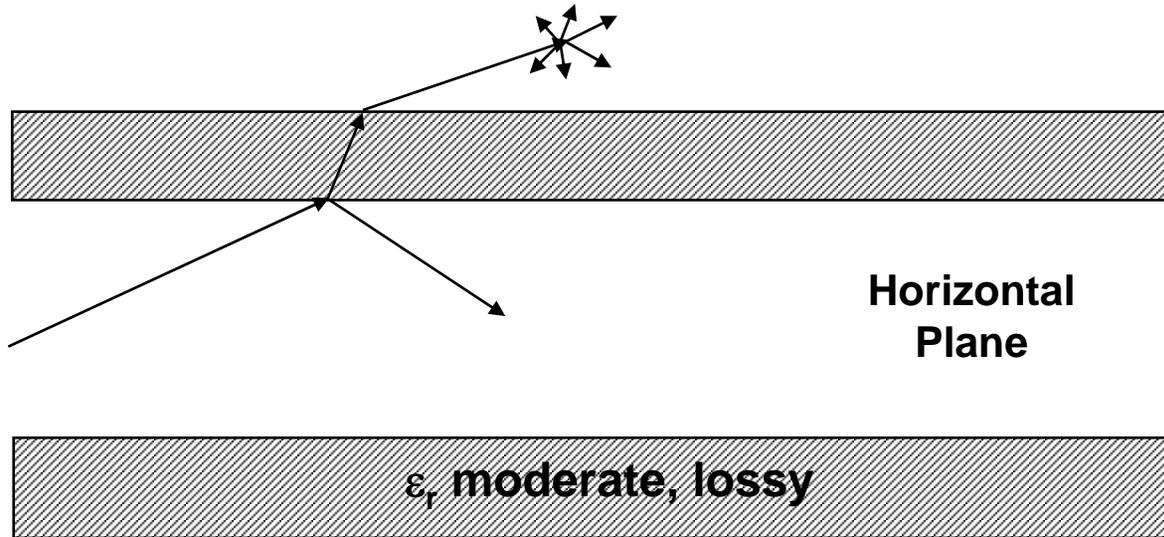


Vertical Plane:

- Efficient Containment,
- Lossy propagation due to horizontal plane loss,
- Low-order modes propagate best



How Hallways Can be a Headache (2)



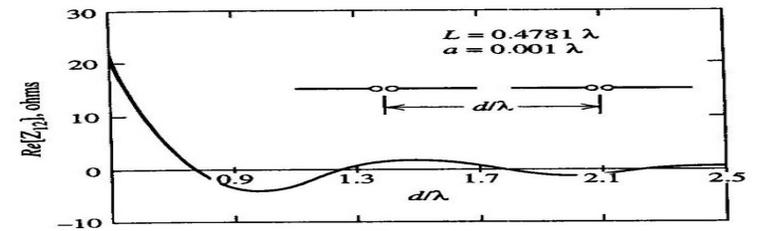
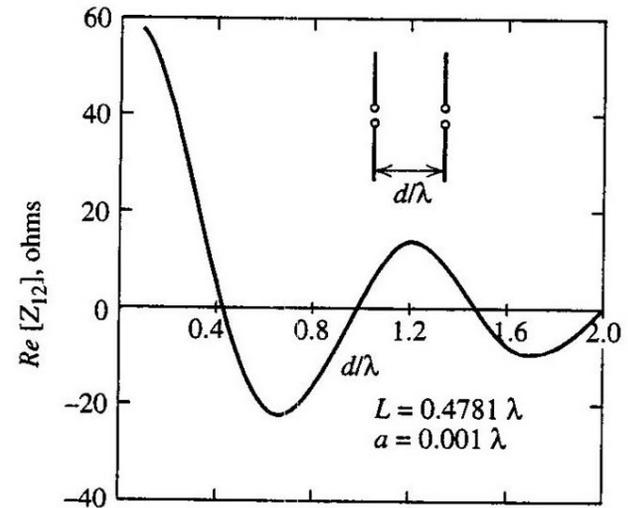
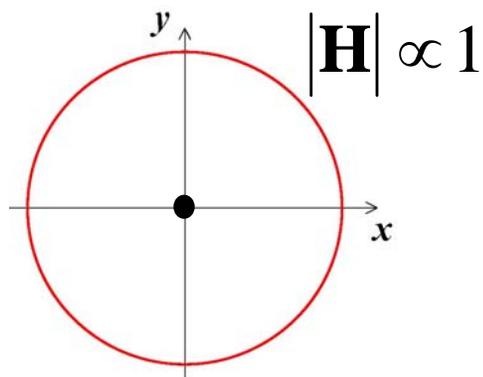
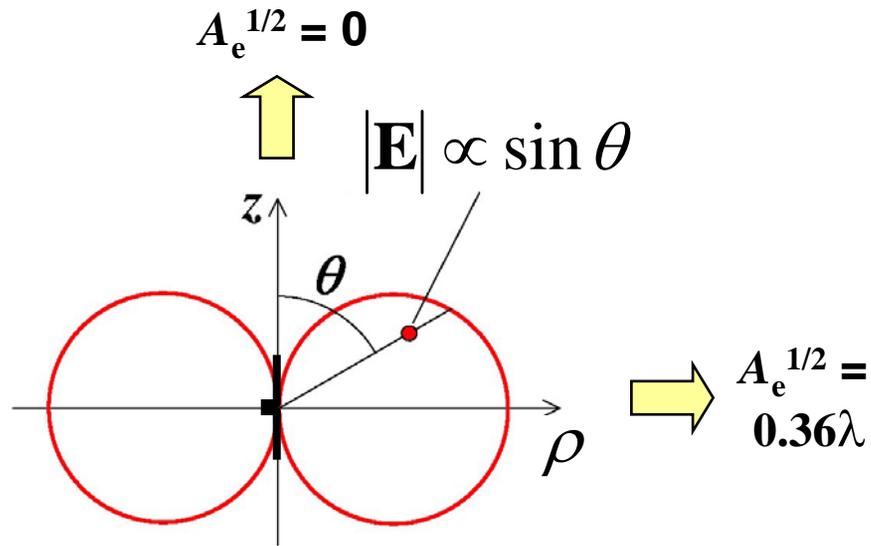
Hallway Countermeasures

- **Short links (<10 m or so at 2.4 GHz)**
- **Distributed arrays (Single elements widely spaced)**
- **Vertical or 2D distribution of array elements**

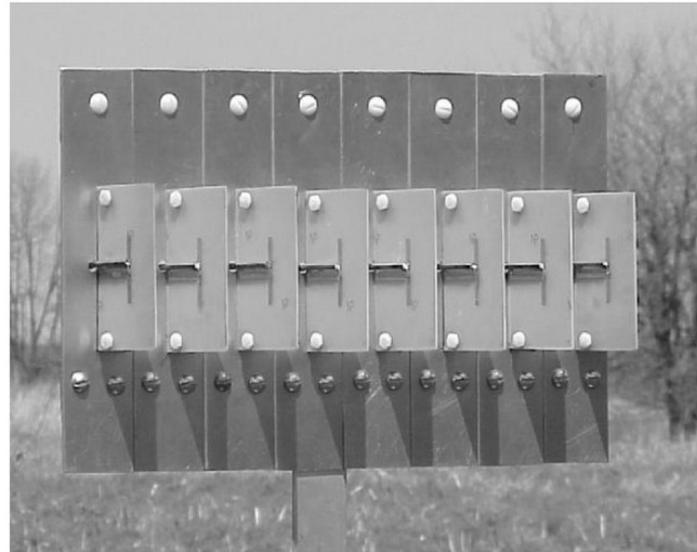
Summary

- **Take care of CNR first, rank-1 diversity second, then think MIMO**
 - **Spatial diversity is very important... Indoor channels - including MIMO subchannels - always experience flat fading**
- **An array that is well-designed from a CNR and diversity perspective will tend be suitable for whatever MIMO subchannels can be found**
- **It is not sufficient to simply find MIMO subchannels; they must be received with sufficient SNR and diversity to significantly contribute to the capacity.**
 - **It is easy to be fooled by techniques such as SNR normalization**

Resonant Half-Wave Dipoles as Elements



Pattern Modification from Mutual Coupling



HWD's spaced about 0.5λ apart at 2.4 GHz
(1.4 relative to $A_e^{1/2}$)

Fig. 1. Photograph of an eight-element linear array of printed dipoles.

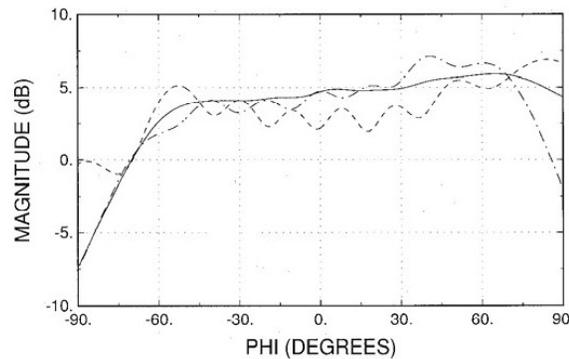


Fig. 2. Radiation pattern of element #1 of the linear array of dipoles at 2.45 GHz. (—) measured pattern, (---) predicted pattern with the single element in front of the small plate, and (- · - ·) predicted pattern with the single element in front of the large plate.

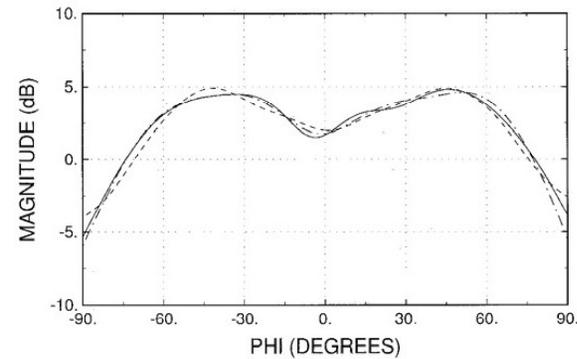
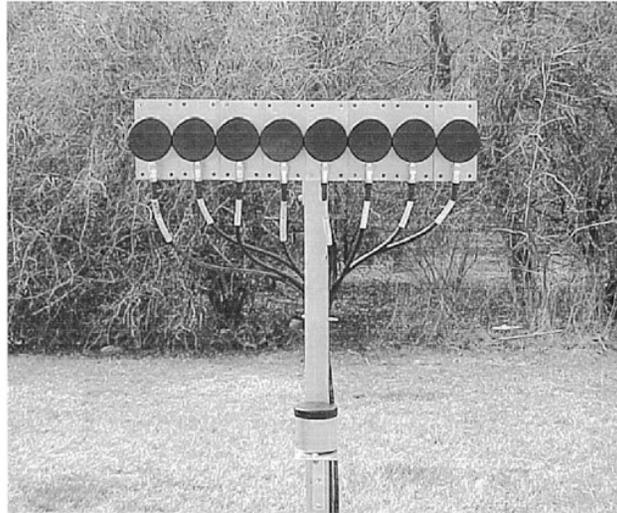


Fig. 3. Radiation pattern of element #4 of the linear array of dipoles at 2.45 GHz. (—) measured pattern, (---) predicted pattern with the single element in front of the small plate, and (- · - ·) predicted pattern with the single element in front of the large plate.

Pattern Modification from Mutual Coupling



Cylindrical horn
antennas spaced
about 0.7λ apart at 2.4
GHz
(7.8 relative to $A_e^{1/2}$)

Fig. 4. Photograph of an eight-element linear array of model P-2406 antennas.

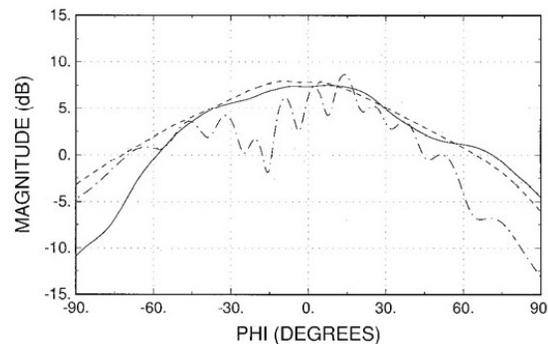


Fig. 5. Radiation pattern of element #1 of the linear array of model P-2406 antennas at 2.45 GHz. (—) measured pattern, (---) predicted pattern with identity coupling matrix, and (- · - ·) predicted pattern with calculated coupling matrix.

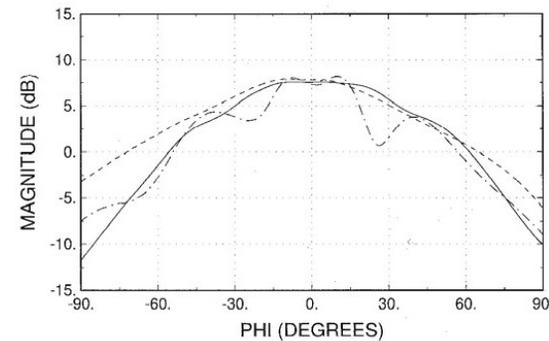


Fig. 6. Radiation pattern of element #4 of the linear array of model P-2406 antennas at 2.45 GHz. (—) measured pattern, (---) predicted pattern with identity coupling matrix, and (- · - ·) predicted pattern with calculated coupling matrix.