

# Decomposition of Boron Trifluoride in the RF Plasma Environment

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Boron trifluoride (BF<sub>3</sub>) is the most commonly used gas for implanting ions of the N-type dopant boron. BF<sub>3</sub> is non-flammable and does not support combustion, but is toxic when inhaled and corrosive to the skin. A radio frequency (RF) plasma system used to decompose BF<sub>3</sub> was examined. The BF<sub>3</sub> decomposition fractions ( $\eta_{BF_3}$ ) were determined in effluent gas streams of BF<sub>3</sub>/CH<sub>4</sub>/Ar, BF<sub>3</sub>/O<sub>2</sub>/Ar and BF<sub>3</sub>/O<sub>2(glass)</sub>/Ar plasma systems. The by-products detected in the BF<sub>3</sub>/CH<sub>4</sub>/Ar plasma system were CO, CO<sub>2</sub>, SiF<sub>4</sub>, HF and boron-carbon compounds. The by-products detected in the BF<sub>3</sub>/O<sub>2</sub>/Ar plasma system were B<sub>2</sub>O<sub>3(s)</sub> and SiF<sub>4</sub>. The  $\eta_{BF_3}$  in the BF<sub>3</sub>/CH<sub>4</sub>/Ar plasma system was 49.8%, higher than that in the BF<sub>3</sub>/O<sub>2</sub>/Ar and BF<sub>3</sub>/O<sub>2(glass)</sub>/Ar plasma system. However, the amount of decomposed BF<sub>3</sub> divided by the input energy ( $E_{BF_3}$ , energy efficiency) in the BF<sub>3</sub>/O<sub>2(glass)</sub>/Ar plasma system was greater than that in the BF<sub>3</sub>/CH<sub>4</sub>/Ar and BF<sub>3</sub>/O<sub>2</sub>/Ar plasma systems. Moreover, the photo images of depositions of different reacting gases O<sub>2</sub>, H<sub>2</sub> with BF<sub>3</sub> were also compared. The reaction in the BF<sub>3</sub>/O<sub>2</sub>/Ar plasma system generated B<sub>2</sub>O<sub>3</sub> fine particles and led to the deposition of a white substance on the surface of the reactor. The  $\eta_{BF_3}$  was only around 25% for mixing with O<sub>2</sub>, even when the input power exceeded 120 Watts, but the generation of fine particles in the system warrants much more investigation.

**Keywords:** BF<sub>3</sub>, RF plasma, B<sub>2</sub>O<sub>3</sub>, fine particle

## 1. Introduction

Fluorides are effective and widely used as fire suppressants (Noto et al., 1996; Linteris et al., 1996), chemical extinguishers (Babushok et al.,

1996) and ozone-depleting substances (Hayman et al., 1997; Holmes et al., 1996). Additionally, various fluorides have been used in the semiconductor industry, in such techniques as chemical vapor deposition (CVD) (Smith et al., 1998; Schmidt et al., 1998), chemical etching (Leech et al., 1998) and ion implantation (Josep et al., 1999). These hazardous and reactive materials raised environmental, safety and handling issues. Boron trifluoride (BF<sub>3</sub>) is an inorganic fluorinated,

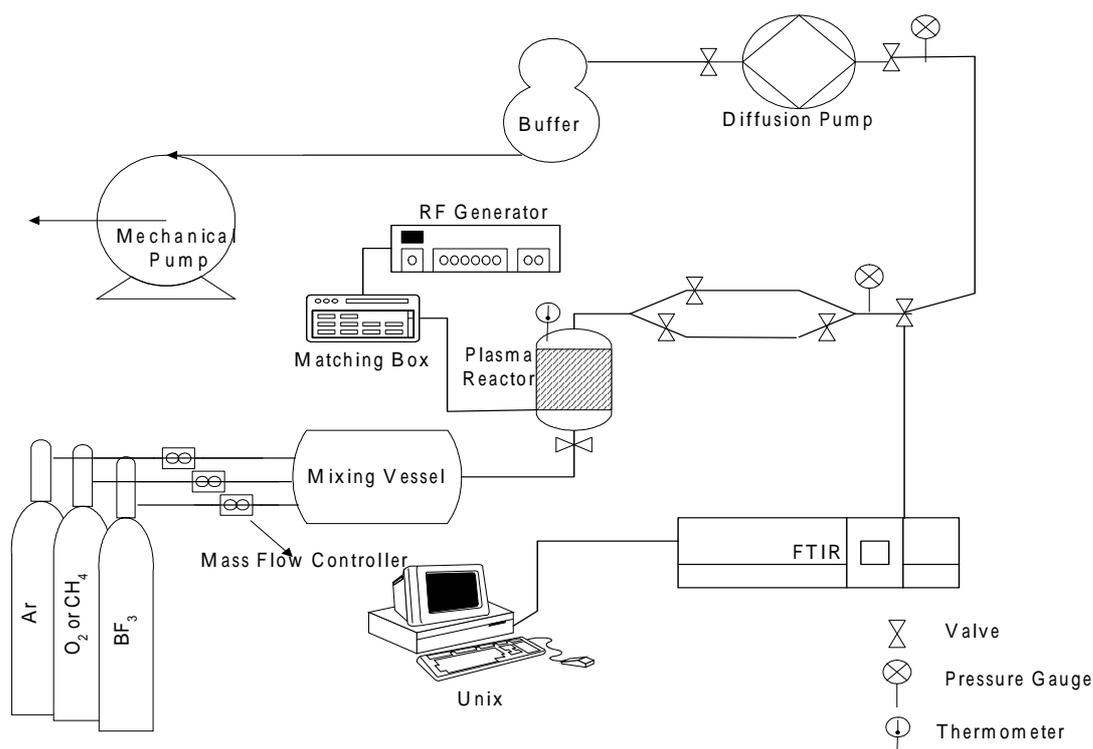
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**Figure 1.** Schematic of the BF<sub>3</sub> RF plasma system

highly toxic, colorless and nonflammable has used to catalyze several chemical reactions, including polymerization, alkylation and acylation. It is also used to detector neutrons and is often used in ion implantation in the semiconductor industry (Schmidt *et al.*, 1998; Boenig, 1988). Ion implantation is a process by which ionized atoms are accelerated directly into a substrate to selectively add dopant atoms. Although the requirements of clearance for semiconductor manufacturing, the generation of fine particles during the process of ion implantation warrants much more attention. The emissions of BF<sub>3</sub> must be controlled because at an immediate danger to live and health (IDLH) of 10 ppm and at a threshold level value (TLV) of 1 ppm, respectively (Josep *et al.*, 1999).

A radio-frequency (RF) plasma environment with a high electrical and thermal conductivity constitutes an excellent energy conversion and heat transfer medium for reactants and products (Hsieh

*et al.*, 1998). The technology provides a more complete and a lower-temperature reaction environment for gas molecules than other methods. However, RF plasma exists out of equilibrium and is often called cold plasma (Boenig, 1988). The kinetic energy of electrons and ions exceeds that of molecules in the cold plasma system. The apparent operating temperature in an RF plasma reactor is generally below 400 °C, while the real temperature of the electrons therein exceeds 2000 °C. Consequently, conventional reactions that must proceed at a very high temperature can be completed at a lower temperature in the RF plasma reactor (Hsieh *et al.*, 1998). Besides, RF plasma does not cause the erosion or corrosion of electrodes by by-products such as HCl or HF, unlike DC plasma (Breitbarth *et al.*, 1997).

Although controlling and reducing the emission of perfluorocompounds (PFCs) has received considerable attention, the decomposition of BF<sub>3</sub> has seldom been addressed. This work compares

the depositions of various reacting gases, O<sub>2</sub>, H<sub>2</sub> with BF<sub>3</sub> in an RF plasma system. Additionally, the effect of input power on the BF<sub>3</sub> decomposition fraction ( $\alpha_{BF_3}$ ) in the BF<sub>3</sub>/CH<sub>4</sub>/Ar, BF<sub>3</sub>/O<sub>2</sub>/Ar and BF<sub>3</sub>/O<sub>2(glass)</sub>/Ar (with glass beads added) RF plasma system was determined. Finally, the possible reaction equations in the BF<sub>3</sub>/CH<sub>4</sub>/Ar and BF<sub>3</sub>/O<sub>2</sub>/Ar RF plasma reactors were proposed.

## 2. Experimental Apparatus

Figure 1 schematically depicts the experimental apparatus used in this study. The BF<sub>3</sub>/CH<sub>4</sub>/Ar or BF<sub>3</sub>/O<sub>2</sub>/Ar mixing gas was metered using Brooks type 5850E mass flow controllers, at a total flow rate of 700 sccm : the gas entered a mixing vessel and was introduced perpendicularly into a 4.14 × 15 cm cylindrical glass reactor. The RF plasma discharge was produced using a plasma generator (PFG 600 RF, Fritz Huttinger Elektronik GmbH) at 13.56 MHz and with a matching network (Matchbox PFM). RF power was delivered through the power meter and the matching unit to an outer copper electrode that was wrapped around the reactor, the other electrode was earthed. The system was inductively coupled : the external electrode and the glass reactor wall beneath it, together with the conductive plasma inside the reactor, generated a capacitor that enabled capacitive coupling of RF power into the discharge (Biederman et al., 1992).

Before the experiment, a diffusion pump was used to maintain the pressure of the system below 0.001 Torr to clean up contamination. Under each designed experimental condition, the input power, the CH<sub>4</sub>/BF<sub>3</sub> or O<sub>2</sub>/BF<sub>3</sub> ratio, the operational pressure and the BF<sub>3</sub> feeding concentration were measured more than three times within five minutes to ensure that steady-state conditions had been reached. Both reactants and final products were first identified by gas chromatography/mass spectrometry (HP5890A PLUS GC/MS). Then, all

species were identified and quantified using an on-line Fourier Transform Infrared (FTIR) spectrometer (Thermo Nicolet AVATRA 360).

Gaseous reactants and products were calibrated by withdrawing unreacted gases and passing them through the sampling line connected to the FTIR. The mass of species was calculated by comparing the response factor (absorbance height/concentration) of standard gas and reaction gas at given IR wave number. Each run of the experiment took 20 min and the results indicated that the steady-state conditions were reached in the effluent after 10 min. The data presented herein are mean values measured after a steady-state condition had been reached.

## 3. Results and Discussion

Experiments were performed to determine the dependence of the BF<sub>3</sub> decomposition fraction ( $\alpha_{BF_3}$ ). The  $\alpha_{BF_3}$  was defined as follows:

$$\alpha_{BF_3} (\%) = [(C_{in(BF_3)} - C_{out(BF_3)}) / C_{in(BF_3)}] * 100\% \quad (1)$$

$C_{in(BF_3)}$  : feeding concentration of BF<sub>3</sub> (%)

$C_{out(BF_3)}$  : effluent concentration of BF<sub>3</sub> (%)

$$\alpha_{CH_4} (\%) = [(C_{in(CH_4)} - C_{out(CH_4)}) / C_{in(CH_4)}] * 100\% \quad (2)$$

$C_{in(CH_4)}$  : feeding concentration of CH<sub>4</sub> (%)

$C_{out(CH_4)}$  : effluent concentration of CH<sub>4</sub> (%)

$$E_{BF_3} = (M_{BF_3} * N * 60 * 1000) / W \quad (3)$$

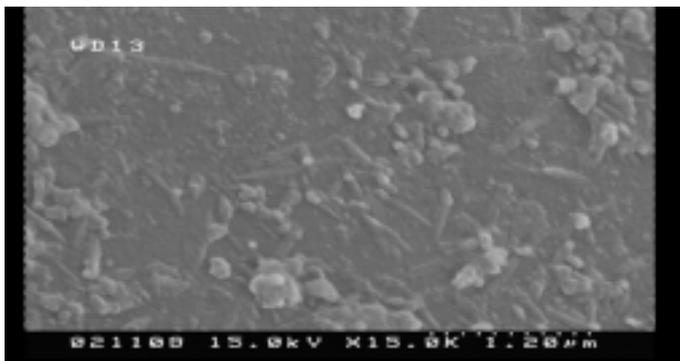
$E_{BF_3}$  : energy efficiency, the amount of decomposed BF<sub>3</sub> divided by the input energy (molecules/kWh)

$M_{BF_3}$  : number of moles of decomposed BF<sub>3</sub>

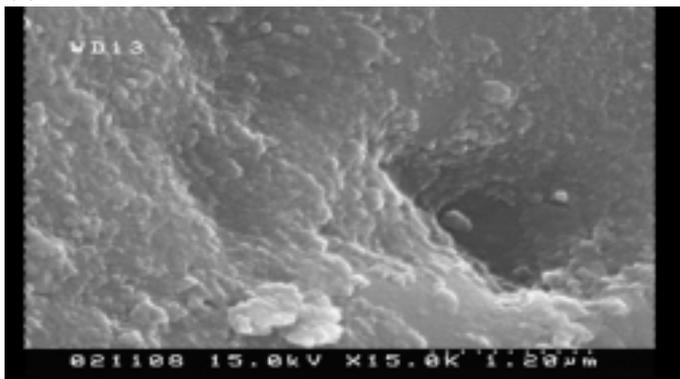
$N$  : Avogadro's number,  $6.02 * 10^{23}$

$W$  : input power (Watts)

$$F_{CO+CO_2} (\%) = [C_{CO} + C_{CO_2} / C_{in(CH_4)}] * 100\% \quad (4)$$



(a) before reaction



(b) after reaction

**Figure 2.** SEM image of glass bead (a) before and (b) after reaction in the BF<sub>3</sub>/O<sub>2</sub>(glass)/Ar system

F<sub>CO+CO<sub>2</sub></sub> : fraction of total input carbon converted into CO and CO<sub>2</sub> (%)

C<sub>CO</sub> : effluent concentration of CO (%)

C<sub>CO<sub>2</sub></sub> : effluent concentration of CO<sub>2</sub> (%)

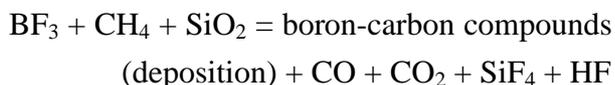
$$F_{SiF_4} (\%) = [C_{SiF_4} * 4 / C_{in(BF_3)} * 3] * 100\%$$

F<sub>SiF<sub>4</sub></sub> : fraction of total input fluorine converted into SiF<sub>4</sub> (%)

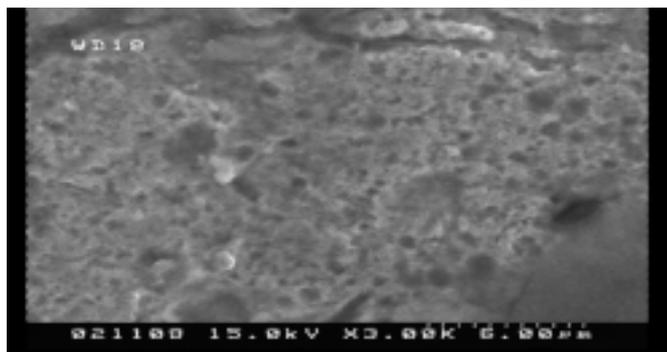
C<sub>SiF<sub>4</sub></sub> : effluent concentration of SiF<sub>4</sub> (%)

### 3.1 Deposition in the BF<sub>3</sub>/CH<sub>4</sub>/Ar Plasma System

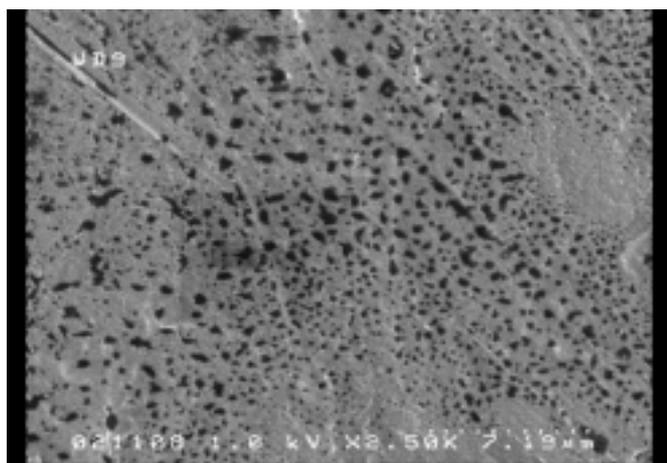
A possible reaction equation of BF<sub>3</sub>/CH<sub>4</sub>/Ar RF plasma system is as follows.



SiF<sub>4</sub> was formed in the well-known plasma-



**Figure 3.** SEM image of deposition in the BF<sub>3</sub>/O<sub>2</sub>/H<sub>2</sub>/Ar system

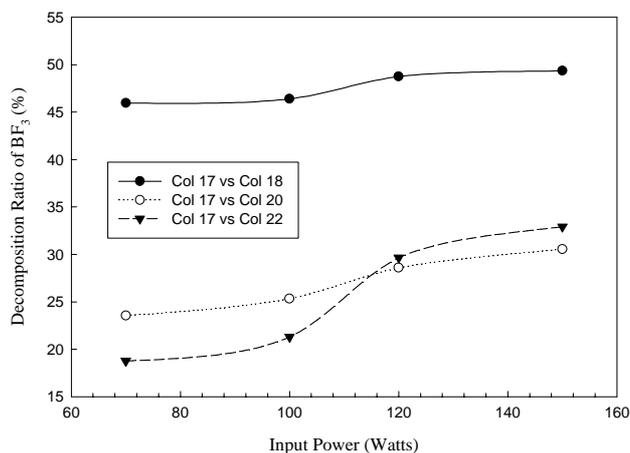


**Figure 4.** SEM image of deposition in the BF<sub>3</sub>/H<sub>2</sub>/Ar system with tungsten as catalyst

chemical etching reaction : SiO<sub>2</sub> + 4F = SiF<sub>4</sub> + O<sub>2</sub>. The SiF<sub>4</sub> was converted into CaF<sub>2</sub> according to the results proposed by Breitbarth, et al. (1997). Additionally, the produced O<sub>2</sub> will react further with CH<sub>4</sub>, resulting in the formation of CO and CO<sub>2</sub> in the RF plasma system. HF was formed because of the high bond strength of H-F (567.9 ± 0.1 D<sub>298</sub><sup>0</sup>/kJ mol<sup>-1</sup>), and reduces the opportunities for reaction between F and C atoms to generate other fluorinated compounds. However, scrubbing or neutralizing easily removed the HF.

A little deposition occurred on the inside of the plasma reactor. The result of Electron Spectroscopy for Chemical Analysis (ESCA, ESCA-210) analysis revealed that carbon, boron, fluorine and silicon were present in the deposition.

### 3.2 Deposition in the BF<sub>3</sub>/O<sub>2</sub>/Ar Plasma System

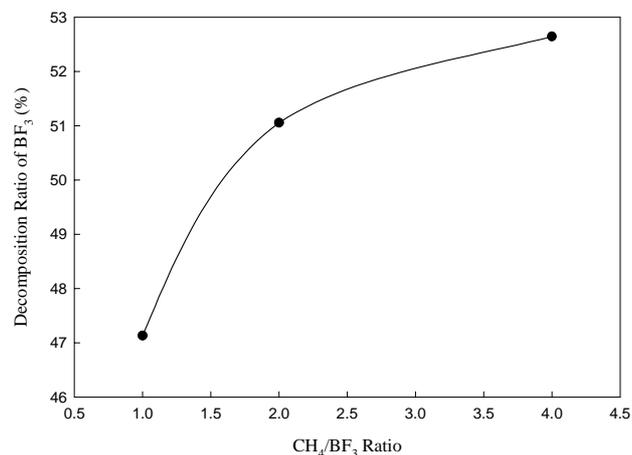


**Figure 5.** Comparison of variation of  $\text{BF}_3$  decomposition ratio with input power among  $\text{BF}_3/\text{CH}_4/\text{Ar}$ ,  $\text{BF}_3/\text{O}_2/\text{Ar}$  and  $\text{BF}_3/\text{O}_2(\text{glass})/\text{Ar}$  RF plasma systems

A possible reaction equation of the  $\text{BF}_3/\text{O}_2/\text{Ar}$  RF plasma system is as follows.



Generated  $\text{B}_2\text{O}_3$  particles will adhere to the surface of the reactor and inhibit further plasma-chemical etching. Interestingly, the increased reaction surface area provided by the addition of glass beads increases the decomposition ratio of  $\text{BF}_3$ . The results in Fig 2 display SEM (SEM, JXA840A) images of the glass beads before and after the reaction between  $\text{BF}_3$  and  $\text{O}_2$  in the RF plasma system. The etching in Fig 2(b) was obvious and the deposition of film on the surface of the glass beads was increased. Figure 3 depicts the deposition of  $\text{BF}_3/\text{O}_2/\text{H}_2/\text{Ar}$  system. The competitive reaction between  $\text{O}_2$  and  $\text{BF}_3$  and  $\text{O}_2$  and  $\text{H}_2$  made the deposition thinner than in the  $\text{BF}_3/\text{O}_2/\text{Ar}$  RF plasma system, in which fewer  $\text{B}_2\text{O}_3$  particles were formed. Figure 4 presents the deposition in the  $\text{BF}_3/\text{H}_2/\text{Ar}$  system, with tungsten as a catalyst in the reactor. Interestingly, cobweb deposition formed on the surface of the reactor. Although the  $\text{BF}_3$  was not favorable, many fine particles were still generated in the system, resulting in the formation of deposition on the surface of the reactor. Accordingly, much more attention should be paid to the generation of fine



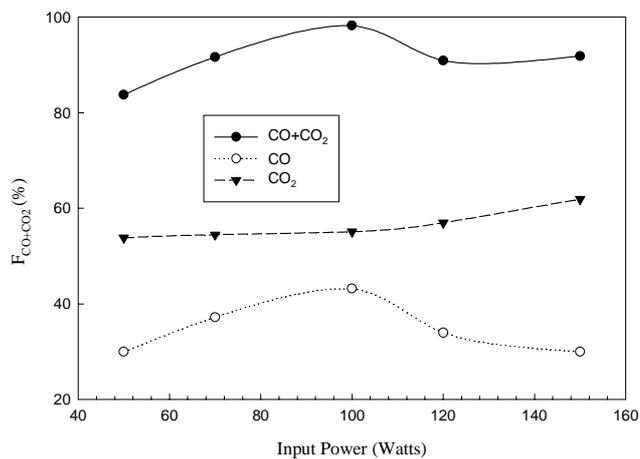
**Figure 6.** Relationship between  $\text{BF}_3$  decomposition ratio and  $\text{CH}_4/\text{BF}_3$  ratio

particles in such systems in the ion implantation industry.

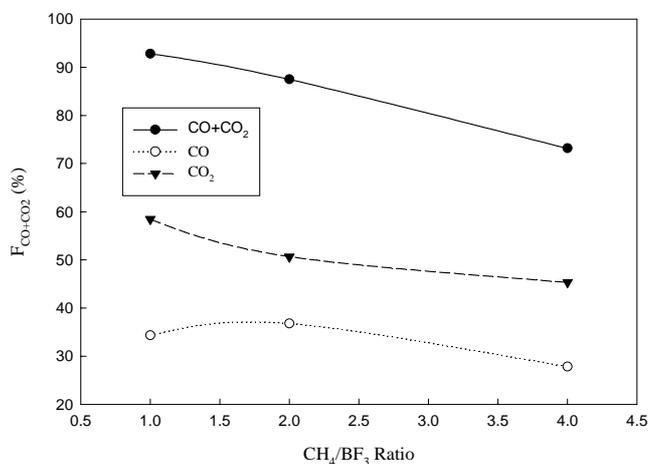
### 3.3 $\text{BF}_3$ and $E_{\text{BF}_3}$ in the $\text{BF}_3$ RF Plasma System

Figure 5 indicated that the values of  $\text{BF}_3$  were 49.8%, 30.5% and 32.9% for  $\text{BF}_3/\text{CH}_4/\text{Ar}$ ,  $\text{BF}_3/\text{O}_2/\text{Ar}$  and  $\text{BF}_3/\text{O}_2(\text{glass})/\text{Ar}$  plasma system, respectively, at an input power of 150 Watts. Accordingly, for a given input power,  $\text{BF}_3$  of the  $\text{BF}_3/\text{CH}_4/\text{Ar}$  plasma system exceeded that of the  $\text{BF}_3/\text{O}_2/\text{Ar}$  or  $\text{BF}_3/\text{O}_2(\text{glass})/\text{Ar}$  plasma system. Moreover,  $\text{BF}_3$  increased when a catalyst (glass beads) was added to the system, when the input power exceeded 120 Watts. The value of  $\text{BF}_3$  increased with the input power,  $\text{BF}_3$  also increased from 47.1% to 52.6% as the  $\text{CH}_4/\text{BF}_3$  ratio increased from 1.0 to 4.0 (Fig 6). Although the  $\text{BF}_3$  is not high enough, the  $\text{CH}_4$  was almost 100% under all experimental conditions. However, the results for  $E_{\text{BF}_3}$  revealed that the energy efficiency was  $2.63 \times 10^{23}$  in the  $\text{BF}_3/\text{O}_2(\text{glass})/\text{Ar}$  plasma system, better than that in the  $\text{BF}_3/\text{O}_2/\text{Ar}$  ( $E_{\text{BF}_3} = 1.77 \times 10^{23}$ ) and  $\text{BF}_3/\text{CH}_4/\text{Ar}$  ( $E_{\text{BF}_3} = 1.48 \times 10^{21}$ ) plasma systems, respectively.

### 3.4 Detecting Products in the $\text{BF}_3/\text{CH}_4/\text{Ar}$ Plasma System

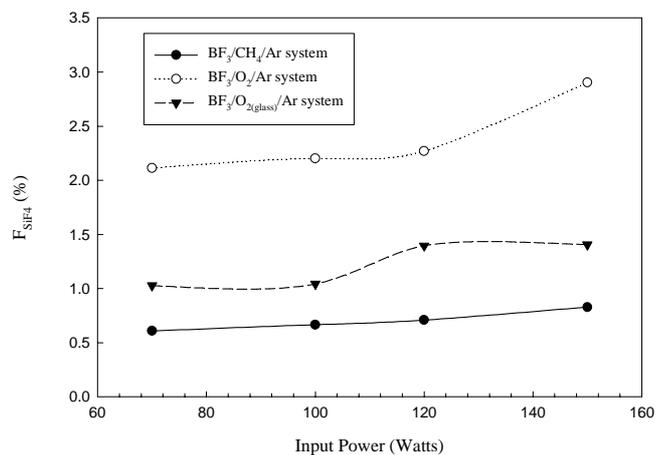


**Figure 7.** Fraction of total input carbon converted into CO and CO<sub>2</sub> in the BF<sub>3</sub>/CH<sub>4</sub>/Ar RF plasma system

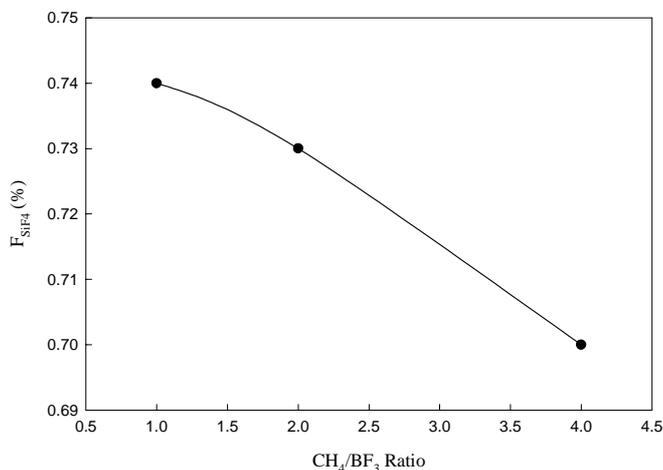


**Figure 8.** Relationship between fraction of total input carbon converted into CO and CO<sub>2</sub> and the CH<sub>4</sub>/BF<sub>3</sub> ratio

According to Fig 7, the fraction of total input carbon converted into CO (F<sub>CO</sub>) increased from 29.9% to 43.1%, and then declined to 29.9% as the input power increased from 50 to 150 Watts. The fraction of total input carbon converted into CO<sub>2</sub> (F<sub>CO<sub>2</sub></sub>) increased from 53.8% to 61.9% as the input power increased from 50 to 150 Watts. The value of F<sub>CO+CO<sub>2</sub></sub> increased from 83.7% to 98.2% and then declined to 91.8% as the input power increased. However, Fig. 8 indicated that F<sub>CO</sub> increased from 34.4% to 36.8% and then fell to 27.9% as the CH<sub>4</sub>/BF<sub>3</sub> ratio increased from 1.0 to 4.0. The value of F<sub>CO<sub>2</sub></sub> fell from 58.4% to 45.3% as the CH<sub>4</sub>/BF<sub>3</sub> ratio increased from 1.0 to 4.0. The value of F<sub>CO+CO<sub>2</sub></sub> declined from 92.8% to 73.2% as the



**Figure 9.** Comparison of the fraction of total input fluorine converted into SiF<sub>4</sub> with input power among BF<sub>3</sub>/CH<sub>4</sub>/Ar, BF<sub>3</sub>/O<sub>2</sub>/Ar and BF<sub>3</sub>/O<sub>2(glass)</sub>/Ar RF plasma systems



**Figure 10.** Relationship between the fraction of total input fluorine converted into SiF<sub>4</sub> and the CH<sub>4</sub>/BF<sub>3</sub> ratio

CH<sub>4</sub>/BF<sub>3</sub> ratio increased from 1.0 to 4.0.

The value of F<sub>SiF<sub>4</sub></sub> increased from 0.61% to 0.83%, from 2.11% to 2.90% and from 1.03% to 1.41% for BF<sub>3</sub>/CH<sub>4</sub>/Ar, BF<sub>3</sub>/O<sub>2</sub>/Ar and BF<sub>3</sub>/O<sub>2(glass)</sub>/Ar plasma systems, respectively, as the input power increased from 70 to 150 Watts (Fig 9). The F<sub>SiF<sub>4</sub></sub> was higher in the BF<sub>3</sub>/O<sub>2</sub>/Ar plasma system than in the BF<sub>3</sub>/CH<sub>4</sub>/Ar plasma system, because of the competition between the etching process and the formation of HF. Additionally, the value of F<sub>SiF<sub>4</sub></sub> declined from 0.74% to 0.70% as the CH<sub>4</sub>/BF<sub>3</sub> ratio increased from 1.0 to 4.0 (Fig 10). The value of F<sub>BF<sub>3</sub></sub> was around 50% during mixing

with the CH<sub>4</sub>, but near only 29% during mixing with O<sub>2</sub>, even when the input power exceeded 120 Watts. Although the value of  $\eta_{BF_3}$  in the BF<sub>3</sub>/O<sub>2</sub>/Ar plasma system was lower than that in the BF<sub>3</sub>/CH<sub>4</sub>/Ar plasma system, the generation of fine particles and their deposition were more serious in the BF<sub>3</sub>/O<sub>2</sub>/Ar plasma system, which fact warrants further investigation.

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