

Near-field thermodynamics and nanoscale energy harvesting

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We study the thermodynamics of near-field thermal radiation between two identical polar media at different temperatures. As an application, we consider an idealized energy harvesting process from sources at near room temperature at the nanoscale. We compute the maximum work flux that can be extracted from the radiation in the near-field regime and compare it with the corresponding maximum work flux in the blackbody regime. This work flux is considerably higher in the near-field regime. For materials that support surface phonon polaritons, explicit expressions for the work flux and an upper bound for the efficiency as functions of the surface wave frequency are obtained.

I. INTRODUCTION

Near-field radiative heat transfer has recently attracted much attention due to the important role it plays in nanoscale physics and technology. Thermal radiation heat transfer in this regime is considerably enhanced as compared to the blackbody limit [1–3]. That is, the amount of energy exchanged between bodies separated by submicron distances is notably higher than that for bodies separated by macroscopic distances [4–6]. The tunneling of evanescent electromagnetic waves is responsible for this enhancement, an effect that can rise only when the bodies are close to each other [7, 8]. This phenomenon is exploited, for instance, in scanning thermal microscopy [9, 10], the recently developed near-field thermal transistor [11], and the generation of usable energy from thermal sources via thermophotovoltaic devices [12–16]. Due to the contribution of evanescent modes, the local density of states is modified close to an interface separating two media [17]. This implies that the thermodynamic functions will also depend on this contribution [18, 19] and will show a very different behavior from the one shown in the far-field case.

Here we consider the thermodynamics of near-field thermal radiation and its application to energy harvesting. We focus on the radiation emitted by two identical polar media at different temperatures and compute the maximum work that can be extracted from this system. An upper bound for the efficiency is also discussed. Here we concentrate on the case where the temperature difference between the hot source and the receiver is small. In these conditions, on the one hand, converters working in the far field not only have low efficiencies, but also the power they supply is poor. This is due to the fact that converters in the far field require high temperature sources to operate in optimal conditions [20]. On

the other hand, although the efficiency remains low if the temperature difference between the source and the receiver is small, the delivered power is notably higher for converters working in the near field. Thus, near-field radiation brings out the possibility for energy harvesting from sources of moderate temperature at the nanoscale.

II. FLUCTUATING FIELDS AND ENERGY FLUX

Near-field radiative heat transfer is described using a semi-classical approach. That is, the classical Maxwell equations are utilized to describe the electromagnetic fields produced by currents in the material, while quantum statistics is introduced to account for the characteristic occupation numbers of photons in energy levels. Such an approach is known as fluctuating electrodynamics [21]. The currents in the material are due to the random movement of charges associated to thermal excitations. That is, thermal radiation is produced by stochastic fluctuations of the currents. Moreover, the Fourier components of the electric and magnetic fields, $\mathbf{E}(\mathbf{r}, \omega)$ and $\mathbf{H}(\mathbf{r}, \omega)$, respectively, can be written in terms of the Fourier components of the current $\mathbf{j}(\mathbf{r}, \omega)$ according to [22, 23]

$$\mathbf{E}(\mathbf{r}, \omega) = i\mu_0\omega \int_V d^3\mathbf{r}' \mathbb{G}^E(\mathbf{r}, \mathbf{r}', \omega) \cdot \mathbf{j}(\mathbf{r}', \omega), \quad (1)$$

$$\mathbf{H}(\mathbf{r}, \omega) = \int_V d^3\mathbf{r}' \mathbb{G}^H(\mathbf{r}, \mathbf{r}', \omega) \cdot \mathbf{j}(\mathbf{r}', \omega), \quad (2)$$

where \mathbb{G}^E and \mathbb{G}^H are the classical electric and magnetic Green tensors, respectively, and μ_0 is the vacuum permeability. The integrations extend over the volume V in the material where the currents are present and these Green tensors relate the source current at point \mathbf{r}' to the electric and magnetic fields at point \mathbf{r} outside the volume. Here we shall restrict ourselves to isotropic nonmagnetic materials.

In neutral materials, the statistical average of the fluctuating charge density and of the electric current density

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vanish. Therefore, also the average value of the fluctuating electromagnetic fields is null. However, although the average values of the fields vanish, their correlations are different from zero. The associated correlation function for the Cartesian components j_k ($k = 1, 2, 3$) of the current is given by the fluctuation-dissipation theorem [7, 24]

$$\langle j_k(\mathbf{r}, \omega) j_l^*(\mathbf{r}', \omega') \rangle = 4\pi\epsilon_0 \hbar \omega^2 n(\omega, T) \text{Im}[\epsilon(\omega)] \times \delta_{kl} \delta(\omega - \omega') \delta(\mathbf{r} - \mathbf{r}'), \quad (3)$$

where $\langle \dots \rangle$ denotes statistical average, ϵ_0 is the permittivity of vacuum, \hbar is the reduced Planck constant, the asterisk denotes the complex conjugate, and $\text{Im}[\epsilon(\omega)]$ denotes the imaginary part of the complex dielectric constant of the medium $\epsilon(\omega)$. Here

$$n(\omega, T) = \left[e^{\hbar\omega/(k_B T)} - 1 \right]^{-1} \quad (4)$$

is the average number of photons in a single mode of frequency ω at equilibrium temperature T , and k_B is the Boltzmann constant. Therefore, given the Green tensors, the expressions for the fields (1) and (2), and the fluctuation-dissipation theorem (3), the average of quantities like the Poynting vector $\Sigma = \mathbf{E} \times \mathbf{H}$ can be computed (see Ref. [7]). The Poynting vector is quadratic in the fields and, hence, its average value does not vanish due to correlations.

Consider now two semi-infinite media with planar surfaces separated by a vacuum gap and with different temperatures; T_1 for medium 1 and T_2 for medium 2. The average of the component of the Poynting vector perpendicular to the surface of the material gives the energy flux (energy per unit time and surface) radiated by the fluctuating currents inside the material. Hence, the energy flux emitted by medium 1 and absorbed by the second medium can be written as

$$\dot{U}(T_1) \equiv \langle \Sigma_z^{1 \rightarrow 2} \rangle = \langle \mathbf{E}_1 \times \mathbf{H}_1 \rangle \cdot \mathbf{e}_z, \quad (5)$$

where z denotes the direction perpendicular to the surface, and \mathbf{e}_z is the unit vector in this direction. On the other hand, the energy emitted by medium 2 and absorbed by medium 1 is given by $\dot{U}(T_2) = \langle \Sigma_z^{2 \rightarrow 1} \rangle$. Furthermore, for a given temperature T , the energy flux can be written as

$$\dot{U}(T) = \int_0^\infty d\omega \hbar \omega n(\omega, T) \varphi(\omega), \quad (6)$$

where $\varphi(\omega)$ is the spectral flux of modes [25]. The net energy transfer $\Delta\dot{U} = \dot{U}(T_2) - \dot{U}(T_1)$ is therefore given by

$$\Delta\dot{U} = \int_0^\infty d\omega \hbar \omega [n(\omega, T_2) - n(\omega, T_1)] \varphi(\omega). \quad (7)$$

The function $\varphi(\omega)$ is well-known for planar surfaces [7, 8, 22, 26]. Considering that the two materials are identical and introducing the reflection coefficients of the

vacuum-material interface $R_\alpha(\kappa, \omega)$ for the polarizations $\alpha = p, s$, the spectral flux of modes is given by

$$\varphi(\omega) = \sum_{\alpha=p,s} \left\{ \int_0^{\omega/c} \frac{d\kappa \kappa}{4\pi^2} \frac{[1 - |R_\alpha(\kappa, \omega)|^2]^2}{|1 - e^{2i\gamma d} R_\alpha^2(\kappa, \omega)|^2} + \int_{\omega/c}^\infty \frac{d\kappa \kappa}{\pi^2} \frac{e^{-2|\gamma|d} \text{Im}^2[R_\alpha(\kappa, \omega)]}{|1 - e^{-2|\gamma|d} R_\alpha^2(\kappa, \omega)|^2} \right\}. \quad (8)$$

Here, d is the separation between the surfaces, c is the speed of light in vacuum, and κ is the component of the wave vector parallel to the surfaces satisfying $\gamma = [(\omega/c)^2 - \kappa^2]^{1/2}$. The quantity γ is the component of the wave vector perpendicular to the surfaces in vacuum. This component of the wave vector in the media depends on the dielectric constant and takes the form $\gamma_m = [(\omega/c)^2 \epsilon - \kappa^2]^{1/2}$. In addition, the reflection coefficients depend on the optical properties of the material under consideration and are given by [7]

$$R_p(\kappa, \omega) = \frac{\epsilon\gamma - \gamma_m}{\epsilon\gamma + \gamma_m}, \quad R_s(\kappa, \omega) = \frac{\gamma - \gamma_m}{\gamma + \gamma_m}. \quad (9)$$

Two different contributions to the flux of modes can be identified in (8): The first term in curly brackets accounts for propagative modes such that $\kappa < \omega/c$, while the second term corresponds to evanescent electromagnetic waves, where $\kappa > \omega/c$. Evanescent modes decay exponentially from the surface of the material, so that their contribution is negligible at relatively large distances. In addition, in order to contribute significantly, these modes have to lie in the range of excited thermal modes given by $n(\omega, T)$. Thermal radiation is thus enhanced if it is measured at distances from the surface much smaller than the thermal wavelength $\lambda_T = c\hbar/k_B T$, which for $T = 300$ K takes the value $\lambda_T = 7.6 \mu\text{m}$. Thus, at room temperature, these effects are appreciable at the nanoscale.

III. ENTROPY FLUX

The entropy flux \dot{S} (entropy per unit time and surface) associated to the radiation emitted by the surface of the material can be obtained from the energy flux by taking into account the usual thermodynamic relations. According to this, \dot{S} must satisfy

$$\frac{1}{T} = \frac{d\dot{S}}{d\dot{U}}. \quad (10)$$

This differential equation can be integrated to give

$$\dot{S}(T) = \int_0^T dT' \frac{1}{T'} \frac{d\dot{U}(T')}{dT'}. \quad (11)$$

Assuming that the spectral flux of modes does not depend on T , the entropy flux (11) becomes [25]

$$\dot{S}(T) = \int_0^\infty d\omega k_B m(\omega, T) \varphi(\omega), \quad (12)$$

where we have introduced

$$m(\omega, T) = [1 + n(\omega, T)] \ln [1 + n(\omega, T)] - n(\omega, T) \ln n(\omega, T). \quad (13)$$

We want to stress that since, in general, the optical properties of the material can depend on temperature, φ can also depend on temperature [15]. Nevertheless, if only variations of entropy flux are considered, (12) can still be used if φ is constant or approximately constant in the considered working temperature range, and arbitrary otherwise (see Appendix). We also emphasize that the expressions (6) and (12) for the energy and entropy fluxes, respectively, rest on the assumption that the emitted radiation is in thermal equilibrium with the radiating body at temperature T .

IV. THERMODYNAMICS OF AN IDEAL ENERGY CONVERSION PROCESS

The conversion of thermal radiation can be seen as the evolution of the photon gas between two different states, in such a way that during its evolution the system delivers some useful work. Instead of having a cyclic machine, in this case the stationary energy and entropy fluxes lead to an stationary usable work flux. The first law of thermodynamics states that

$$\Delta\dot{U} + \dot{Q}_e + \dot{W} = 0, \quad (14)$$

where $\Delta\dot{U}$ is the variation of the internal energy of the photon gas, \dot{Q}_e is the heat flux delivered to the environment during the transformation and \dot{W} is the flux of usable work that can be obtained during the process. Assuming that \dot{Q}_e is transferred isothermally to the environment at temperature T_e , the variation of the entropy flux in the environment is given by $\Delta\dot{S}_e = \dot{Q}_e/T_e$. Thus, T_e is also the temperature of the photon gas in its final state if we assume that it ends in thermal equilibrium with the environment. In addition, the second law of thermodynamics establishes that the variation of the entropy flux in the system $\Delta\dot{S}$ satisfies [27]

$$\Delta\dot{S} + \Delta\dot{S}_e = \Delta\dot{S}_{\text{irr}} \geq 0, \quad (15)$$

where $\Delta\dot{S}_{\text{irr}}$ is the entropy production that accounts for irreversibilities in the process of conversion. Combining (14) and (15), the work flux in the stationary regime can be written as

$$\dot{W} = T_e \Delta\dot{S} - \Delta\dot{U} - T_e \Delta\dot{S}_{\text{irr}}. \quad (16)$$

An ideal process is that for which no entropy is produced due to irreversibilities, $\Delta\dot{S}_{\text{irr}} = 0$. Thus, the ideal work flux \dot{W} delivered by the system during an ideal process is given by [28]

$$\dot{W} \equiv T_e \Delta\dot{S} - \Delta\dot{U}. \quad (17)$$

Of course, real energy conversion processes are not ideal. However, even for a non-ideal process, \dot{W} gives relevant information about the energy conversion since it is the maximum work flux that can be obtained from the system for a given initial state. In our case, the initial state is defined by the temperature of the hotter radiating medium, which we denote by T_h , $T_h > T_e$. According to the previous discussion, the temperature of the second medium is T_e , so that $\Delta\dot{U} = \dot{U}(T_e) - \dot{U}(T_h)$, with the energy flux given by (6). Furthermore, the variation of entropy flux is $\Delta\dot{S} = \dot{S}(T_e) - \dot{S}(T_h)$, and hence

$$\Delta\dot{S} = \int_0^\infty d\omega k_B [m(\omega, T_e) - m(\omega, T_h)] \varphi(\omega). \quad (18)$$

An important parameter that describes the mechanism of energy conversion is the efficiency of the process. For an ideal process, an adequate criterion that quantifies the performance of the conversion is given by the first law efficiency η . Hereafter we denote by $\bar{\eta}$ the efficiency of an ideal process. This can be written as [28]

$$\bar{\eta} = \frac{\dot{W}}{\dot{U}(T_h)}, \quad (19)$$

which is the ratio of the useful work flux to the input energy flux. If the energy conversion process is non-ideal, that is $\Delta\dot{S}_{\text{irr}} \neq 0$, equation (19) still gives information about the process because $\bar{\eta}$ is an upper bound for the efficiency. Below we will consider $\bar{\eta}$ for the case of near-field thermal radiation energy conversion and compare it to the case of blackbody radiation.

V. NEAR-FIELD THERMAL ENERGY HARVESTING

Energy converters can be used with the purpose of capturing thermal energy from their surroundings and transform it into usable work. Here we consider this energy harvesting process in an ideal situation, which is a first approximation to the real case. We consider a semi-infinite medium acting as a thermal energy source at a temperature higher than the environment temperature. This medium could be a certain component of a device which, as a consequence of an independent task, is kept at a working temperature T_h . A second semi-infinite medium is placed near the first one, with a vacuum gap separating the (planar) surfaces of the two media. The second medium is assumed to be in thermal equilibrium with the environment at temperature T_e . Due to the difference of temperatures, it is clear that a certain amount of work can be extracted from the thermal radiation. This function is assigned to the converter, which can be assumed to be coupled to the medium at temperature T_e . The specific mechanism utilized by the converter to transform the radiation will determine the entropy production and, therefore, the efficiency of the process. If this mechanism is not particularized, bounds for

the efficiency and work flux can be obtained by considering an ideal process, as discussed in Sec. IV. These bounds will be obtained below. In particular, we will focus on the case where the difference of temperature between the hot medium and the environment is relatively small. Small temperature differences are the physically relevant situation for energy harvesters at the nanoscale, where near-field thermal radiation is the dominant contribution. In order to quantify the performance of the process in these conditions, we need suitable expressions for the maximum work flux and the upper bound for the efficiency $\bar{\eta}$. Explicitly, a relatively small temperature difference $\Delta T = T_e - T_h$ is achieved if $|\Delta T|/T_0 \ll 1$, with $T_0 = (T_e + T_h)/2$. The maximum usable work flux that an energy harvester can produce is given by (17) and, thus, using (6) and (12), we expand (17) to leading order in ΔT and obtain

$$\dot{W} = \frac{k_B(\Delta T)^2}{2T_0} \int_0^\infty d\omega \left(\frac{\hbar\omega}{k_B T_0} \right)^2 \frac{e^{\hbar\omega/(k_B T_0)} \varphi(\omega)}{[e^{\hbar\omega/(k_B T_0)} - 1]^2}. \quad (20)$$

Notice that energetic and entropic contributions are equal to first order in ΔT , therefore the leading contribution is of order $(\Delta T)^2$. Likewise, a suitable expression for $\bar{\eta}$ will be given below for small gap separations.

As we have seen, the energy transfer strongly depends on the optical properties of the emitters, which are introduced through $\varphi(\omega)$. In what follows we will concentrate on the case of two identical polar media that support surface phonon polaritons, which are surface waves due to the coupling of phononic excitations with the electromagnetic fields [7, 22]. If two planar sources supporting surface phonon polaritons are closely placed, these modes can be resonantly excited and thus produce a considerably increase of the emitted radiation [7, 8]. Examples of materials that support these surface waves are, for instance, silicon carbide (SiC) and hexagonal boron nitride (hBN). The optical properties of these materials can be described by the Lorentz model [16, 29]

$$\varepsilon(\omega) = \varepsilon_\infty \left(\frac{\omega_L^2 - \omega^2 - i\Gamma\omega}{\omega_T^2 - \omega^2 - i\Gamma\omega} \right), \quad (21)$$

where ω_L , ω_T , ε_∞ , and Γ are characteristic parameters of the material. In addition, for these materials, the frequency of the surface phonon polariton of the single interface can be written as [30]

$$\omega_0 = \left(\frac{\varepsilon_\infty \omega_L^2 + \omega_T^2}{\varepsilon_\infty + 1} \right)^{1/2}. \quad (22)$$

Furthermore, in the case of polar materials and when the gap width is small ($d \ll \lambda_T$), the dominant contribution in (8) comes from p-polarized evanescent modes. Retaining only this contribution, the spectral flux of modes in the near-field regime can be obtained using the near-monochromatic approximation and, hence, be written in terms of a Dirac δ distribution as [25, 30]

$$\varphi_{\text{nf}}(\omega) = g_d(\omega)\delta(\omega - \omega_0), \quad (23)$$

where

$$g_d(\omega) = \frac{\text{Re} [\text{Li}_2 (R_p^2(\omega))]}{4\pi d^2 f'(\omega)}. \quad (24)$$

In Eq. (24), we have introduced

$$f(\omega) = \frac{\text{Im} [R_p^2(\omega)]}{\text{Im}^2 [R_p(\omega)]}, \quad (25)$$

with $f'(\omega) = df(\omega)/d\omega$, and $\text{Li}_n(z) = \sum_{k=1}^\infty z^k/k^n$ is the polylogarithm function. The electrostatic limit is also assumed in (23), where the reflection coefficient does not depend on κ and reads

$$R_p(\omega) = \frac{\varepsilon(\omega) - 1}{\varepsilon(\omega) + 1}. \quad (26)$$

It is important to note that the function $g_d(\omega)$ is proportional to $1/d^2$ and, therefore, the thermodynamic quantities in the near-field are functions of the width of the vacuum gap separating the surfaces. We also emphasize that these arguments are valid for polar materials; for metallic surfaces, s-polarized fields dominate the heat transfer [31].

The expression (23) for the spectral flux of modes allows us to compute thermodynamic functions like (20) in the near-field regime. Indeed, to leading order in ΔT we have

$$\dot{W}_{\text{nf}} = \frac{k_B(\Delta T)^2}{2T_0} \left(\frac{\hbar\omega_0}{k_B T_0} \right)^2 \frac{e^{\hbar\omega_0/(k_B T_0)} g_d(\omega_0)}{[e^{\hbar\omega_0/(k_B T_0)} - 1]^2}. \quad (27)$$

In addition, expanding $\dot{U}(T_e) = \dot{U}(T_0 - \Delta T/2)$ about T_0 from (6) with (23), and taking (27) into account, the upper bound for the efficiency (19) in the near-field becomes

$$\bar{\eta}_{\text{nf}} = \frac{\hbar\omega_0(\Delta T)^2}{2k_B T_0^3} \left[1 - e^{-\hbar\omega_0/(k_B T_0)} \right]^{-1}, \quad (28)$$

where, again, we consider only the contribution to leading order in ΔT . For arbitrary temperatures, $\bar{\eta}_{\text{nf}}$ correspond to the efficiency of near-monochromatic radiation [25].

To appreciate the performance of the energy harvesting process in the near-field, it is illuminating to compare (27) and (28) with their analogues in the blackbody regime. In the blackbody regime, the corresponding spectral flux of modes $\varphi_{\text{bb}}(\omega) = \omega^2/(2\pi c)^2$ is obtained by setting $R_\alpha = 0$ in (8). Thus, the ideal work flux in this regime, \dot{W}_{bb} , is obtained from (17) using (6) and (12) with $\varphi(\omega) = \varphi_{\text{bb}}(\omega)$. Notice that using $\varphi(\omega) = \varphi_{\text{bb}}(\omega)$ in (6) leads to the Stefan-Boltzmann law. For small ΔT one obtains $\dot{W}_{\text{bb}} = 2\sigma T_0^2(\Delta T)^2$, where σ is the Stefan constant. In addition, the bound for the efficiency in this case reads [32]

$$\bar{\eta}_{\text{bb}} = 1 - \frac{4}{3} \frac{T_e}{T_h} + \frac{1}{3} \left(\frac{T_e}{T_h} \right)^4. \quad (29)$$

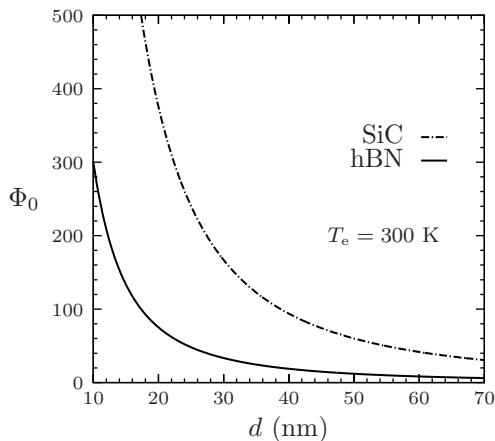


FIG. 1. Ratio $\Phi_0 = \dot{\mathcal{W}}_{\text{nf}}/\dot{\mathcal{W}}_{\text{bb}}$ in the limit where the temperature of the hot source T_h approaches the environmental temperature T_e as a function of the gap width. In this asymptotic limit, the enhancement of the ideal work flux in the near-field regime as compared with that of blackbody radiation is shown for two different materials.

We now define

$$\Phi_0(d, T_e) \equiv \lim_{T_h \rightarrow T_e} \frac{\dot{\mathcal{W}}_{\text{nf}}(d, T_h, T_e)}{\dot{\mathcal{W}}_{\text{bb}}(T_h, T_e)}, \quad (30)$$

which, taking into account the expansions to leading order in ΔT of both $\dot{\mathcal{W}}_{\text{nf}}$ and $\dot{\mathcal{W}}_{\text{bb}}$, can be written as

$$\Phi_0(d, T_e) = \frac{\hbar^2 \omega_0^2}{4\sigma k_B T_e^5} \frac{e^{\hbar\omega_0/(k_B T_e)} g_d(\omega_0)}{[e^{\hbar\omega_0/(k_B T_e)} - 1]^2}. \quad (31)$$

Similarly, in order to compare efficiencies we introduce $\mathcal{R}(T_e) \equiv \lim_{T_h \rightarrow T_e} \bar{\eta}_{\text{nf}}/\bar{\eta}_{\text{bb}}$, which reads

$$\mathcal{R}(T_e) = \frac{\hbar\omega_0}{4k_B T_e} \left[1 - e^{-\hbar\omega_0/(k_B T_e)} \right]^{-1}. \quad (32)$$

The condition $\mathcal{R} > 1$ leads to a threshold frequency $\omega_{\text{th}} = 3.921 k_B T_e / \hbar$ [25]. Thus, if $\omega_0 < \omega_{\text{th}}$, the conversion of near-field radiation cannot be more efficient than the conversion of blackbody radiation at small temperature difference. We stress that ω_0 is a property of the material. The functions Φ_0 and \mathcal{R} are related to each other, with the relation given by

$$\Phi_0(d, T_e) = \frac{\hbar\omega_0}{\sigma T_e^4} g_d(\omega_0) n(\omega_0, T_e) \mathcal{R}(T_e). \quad (33)$$

Of course, both the ideal work flux and the efficiency go to zero in the limit $T_h \rightarrow T_e$. However, the ratios Φ_0 and \mathcal{R} provide intrinsic information about the energy harvesting in the asymptotic limit of small temperature difference. In Fig. 1 we show Φ_0 at $T_e = 300$ K as a function of d for SiC and hBN, where the optical data are taken from [29] for the former material and from [16] for the latter. In the figure it is clearly seen the enhancement in the work flux due to evanescent modes in the near-field regime; $\dot{\mathcal{W}}_{\text{nf}}$ is considerably larger than $\dot{\mathcal{W}}_{\text{bb}}$ at room temperature in the nanoscale.

VI. CONCLUSIONS

We have studied the thermodynamics and energy harvesting of thermal radiation between two semi-infinite polar media separated by a nanoscale vacuum gap in the near-field regime. Thermodynamic functions, such as energy and entropy fluxes, are constructed by computing the spectral flux of modes for the radiation between the surfaces of the materials. The thermodynamic approach and, in particular, the expression for the spectral flux of modes rest on the assumption that the macroscopic Maxwell equations hold at this scale. Thus, although being at the nanoscale, the system is considered to be macroscopic. According to this argument, in principle, there are no reasons to consider finite-size effects in the thermodynamic formalism, as occurs for small systems [33] or for systems with long-range interactions [34]. In small-scale systems, the transport could be affected by forces due to direct interactions between particles, hydrodynamic interactions or excluded volume effects, all these phenomena leading to an emergent dynamics that can be theoretically investigated [35]. In the present case, however, it is the considered thermodynamic system itself, i.e. the electromagnetic radiation, which shows a different behavior at the nanoscale in comparison to the behavior at macroscopic length scales. Such a difference appears here because evanescent modes play a very important role in the nanoscopic vacuum gap, while they are negligible for macroscopic separations. Near-field thermodynamics is, therefore, described by the same thermodynamic relations of macroscopic systems, but with characteristic thermal coefficients containing the small-scale behavior. This formalism can generally be applied to systems that intrinsically modify their nature at non-macroscopic scales. The properties of the system that depend on the working scale are codified in fundamental quantities such as the density of states or the spectral flux of modes. These fundamental quantities are precisely those incorporated in the near-field thermodynamics, as we have shown here.

Furthermore, using the near-monochromatic approximation [30], an analytical expression has been given for the maximum work flux that can be extracted from the radiation in the near field [25]. This quantity has been compared with the one corresponding one to the blackbody regime and is shown to be considerably higher. An upper bound for the thermodynamic efficiency has also been studied. Both maximum work flux and efficiency depend on the optical properties of the materials, and the explicit dependence on the frequency of the surface phonon polariton has been obtained. Since the frequency of the surface waves depends on the choice of the material, our analysis highlights how the properties of the material influence the performance of the energy harvesting process.

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Appendix

We now show that if the spectral flux of modes depends on T but can be considered constant in a certain range of temperatures, equation (18) for the variation of the entropy flux holds if T_e and T_h are in this range. Thus, consider now $\tilde{\varphi} = \tilde{\varphi}(\omega, T)$, so that the energy flux is given by

$$\dot{U}(T) = \int_0^\infty d\omega \hbar\omega n(\omega, T) \tilde{\varphi}(\omega, T). \quad (\text{A.1})$$

According to (11), we have

$$\dot{S}(T) = \int_0^\infty d\omega \hbar\omega \int_0^T \frac{dT'}{T'} \frac{\partial}{\partial T'} [n(\omega, T') \tilde{\varphi}(\omega, T')], \quad (\text{A.2})$$

and therefore $\Delta\dot{S} = \dot{S}(T_e) - \dot{S}(T_h)$ can be written as

$$\Delta\dot{S} = \int_0^\infty d\omega \hbar\omega \int_{T_h}^{T_e} \frac{dT'}{T'} \frac{\partial}{\partial T'} [n(\omega, T') \tilde{\varphi}(\omega, T')]. \quad (\text{A.3})$$

Our assumption here is that

$$\tilde{\varphi}(\omega, T) = \begin{cases} \varphi(\omega) & \text{if } T \in [T_a, T_b], \\ \phi(\omega, T) & \text{otherwise} \end{cases}, \quad (\text{A.4})$$

where $\phi(\omega, T)$ is an arbitrary function. Hence, if both T_e and T_h lie on $[T_a, T_b]$, from (A.3) and (A.4) we obtain

$$\Delta\dot{S} = \int_0^\infty d\omega \hbar\omega \varphi(\omega) \int_{T_h}^{T_e} \frac{dT'}{T'} \frac{\partial n(\omega, T')}{\partial T'}, \quad (\text{A.5})$$

which does not depend on $\phi(\omega, T)$ and is equal to (18) by taking into account the definition of $m(\omega, T)$ given in (13).

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