

Experiments with Balancing on Irregular Terrains using the Dreamer Mobile Humanoid Robot

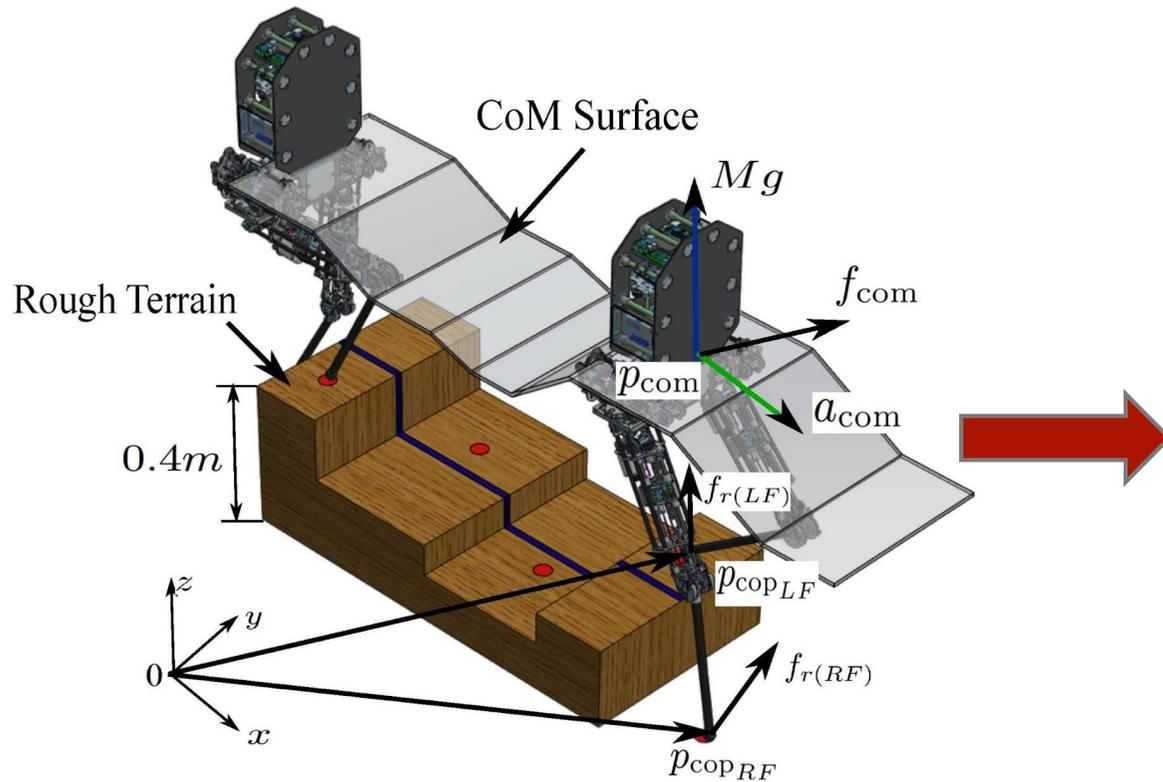
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+ Halmstad University

Robotics Science and Systems
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Motivation



Hume Biped Robot Walking in rough terrain [UT Austin]



Centaur 2 Dexterous Base with Robonaut 2 Upper Body Humanoid [NASA JSC]

From Simulation to Reality: Whole-Body Multicontact Control

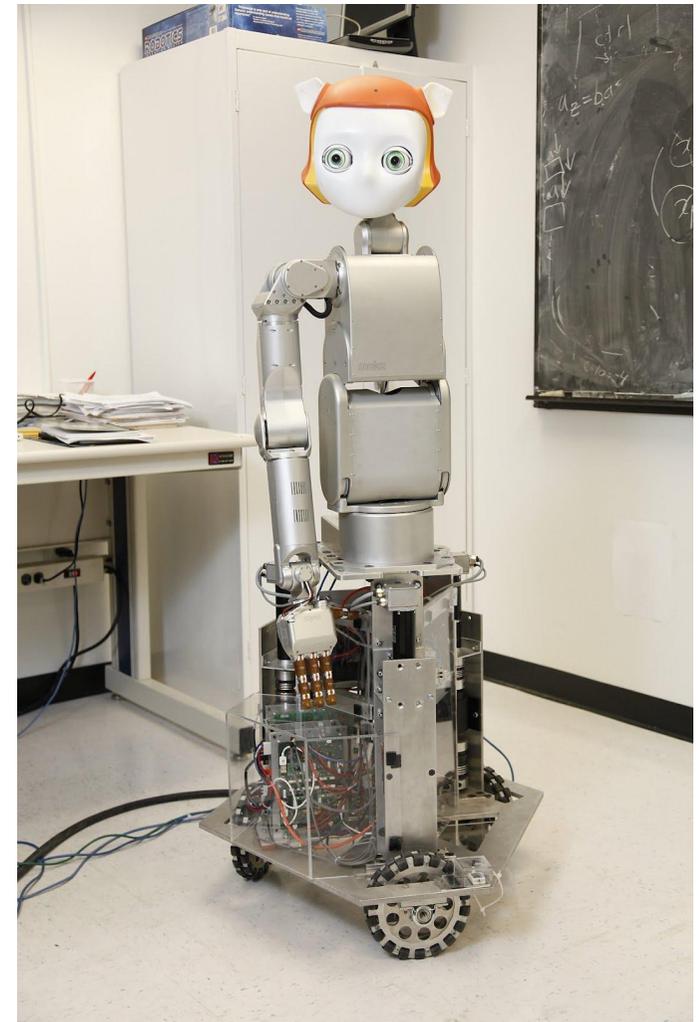
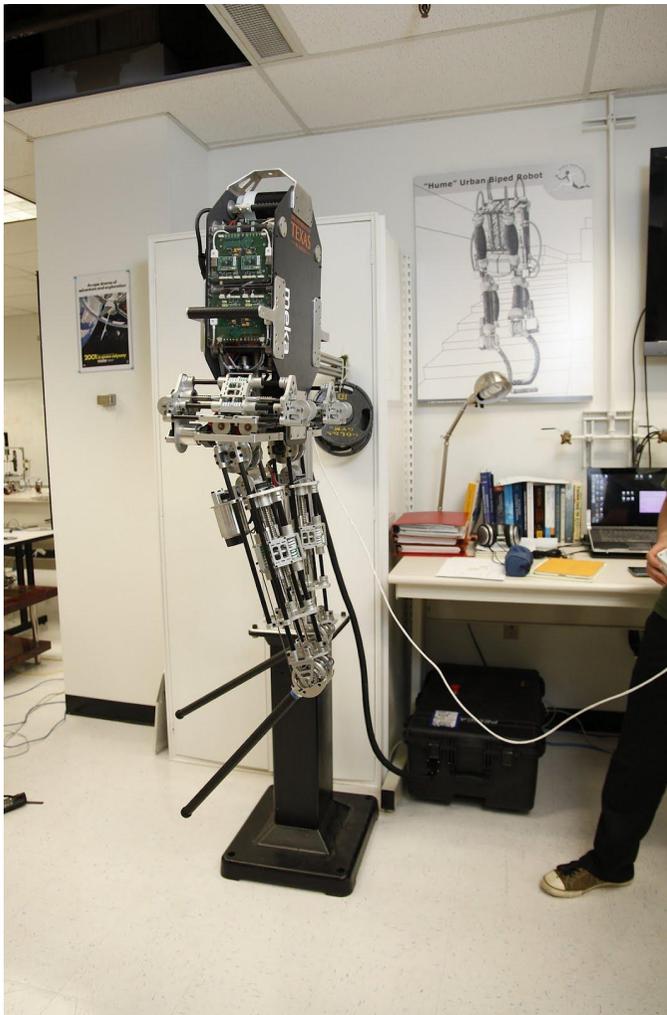
Years 2002-2012

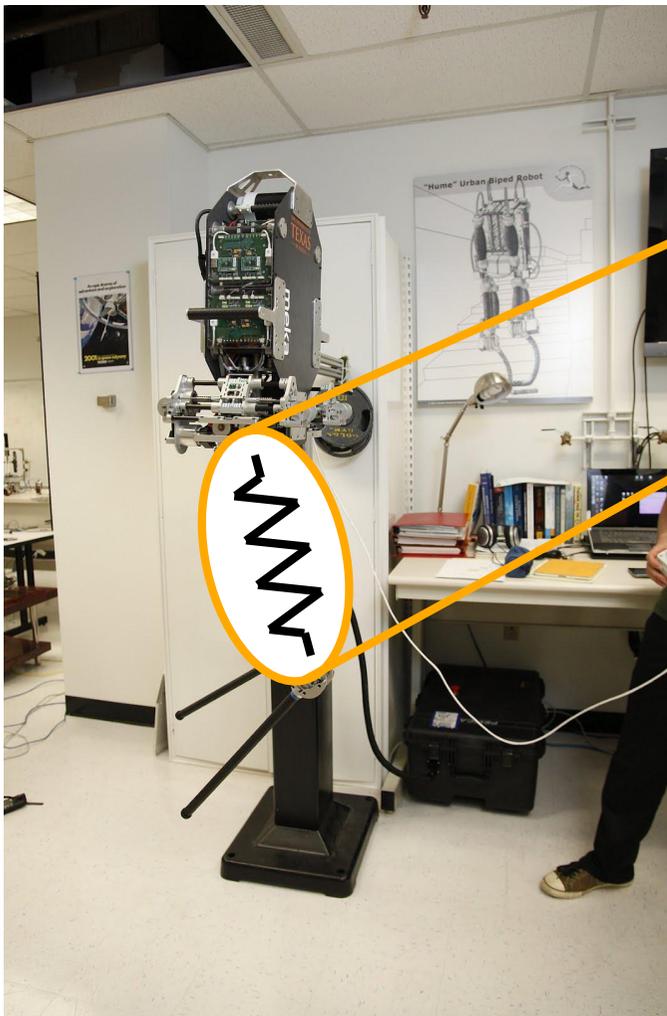
Pursuing Whole-Body
Multicontact Control

Luis Sentis' Contributions at UT
Austin and Stanford University

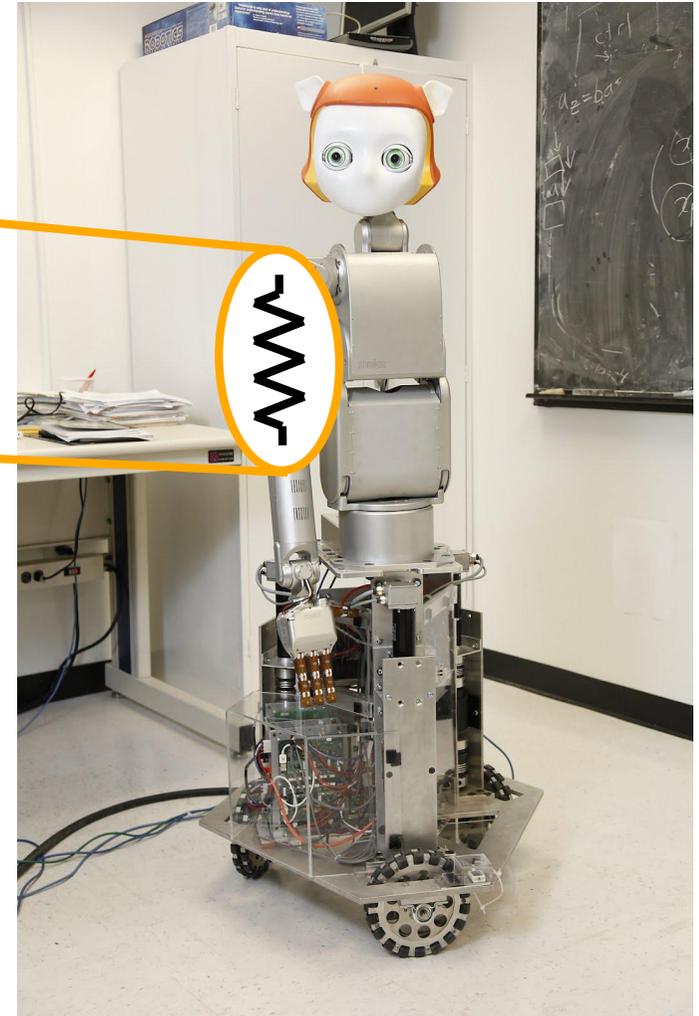
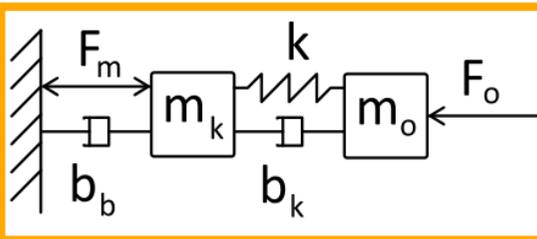


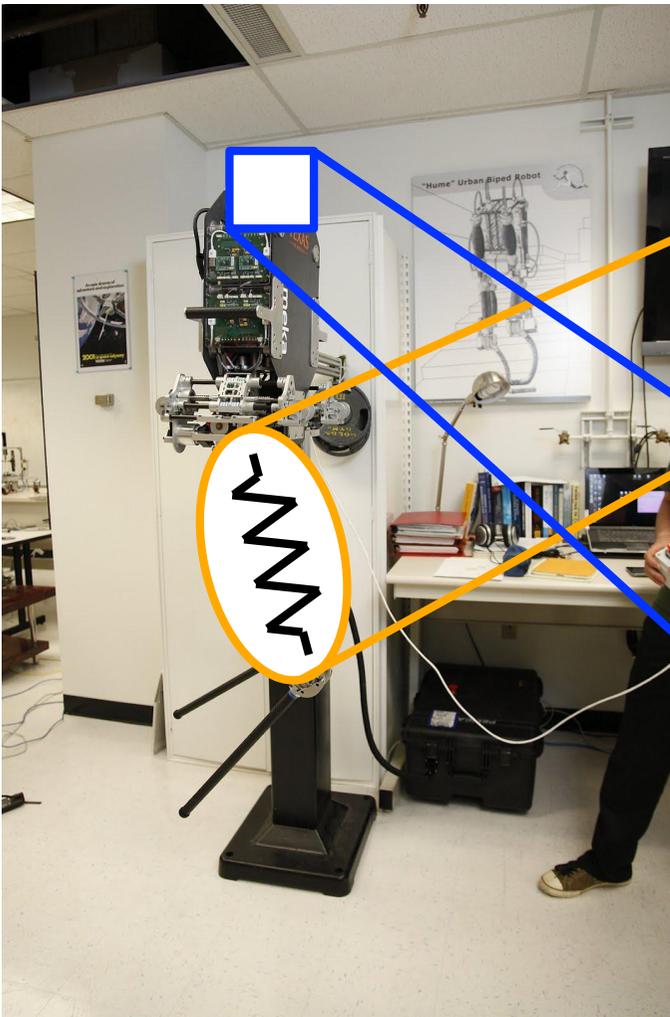
Facilities



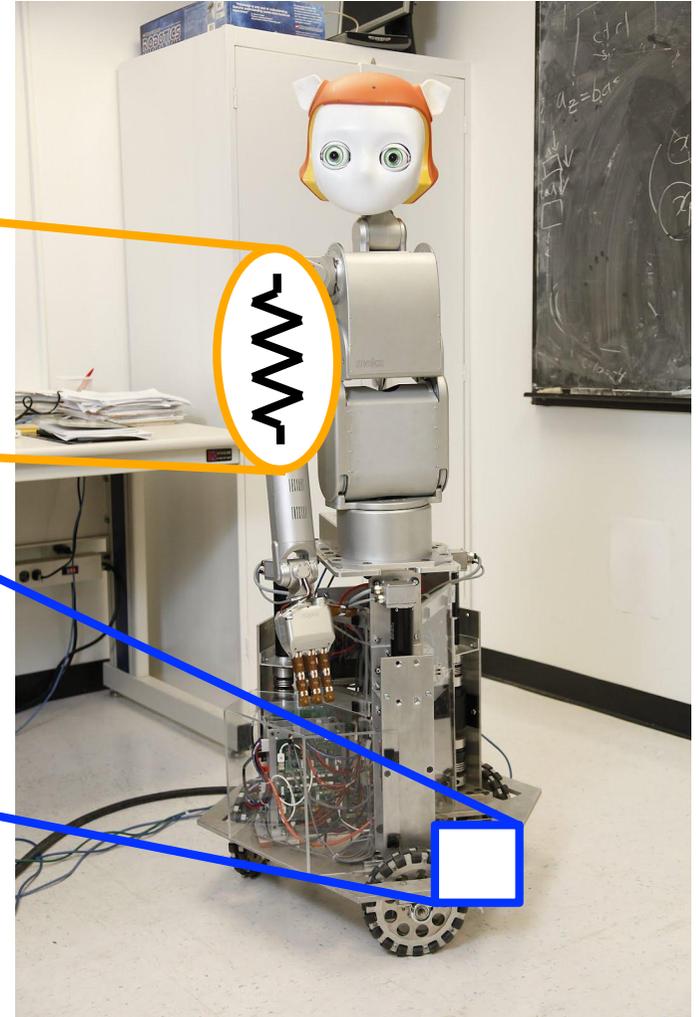
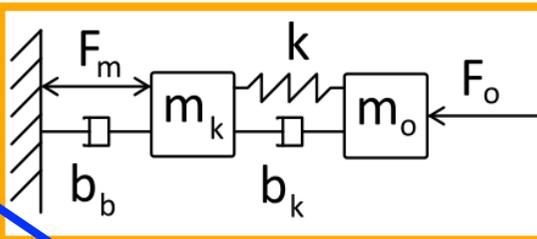


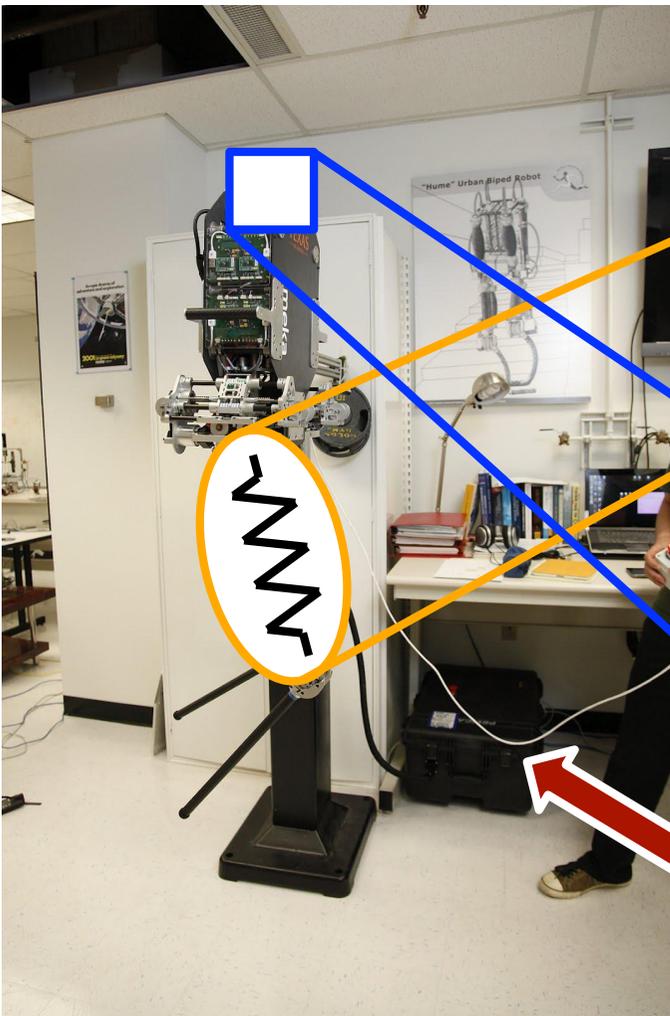
Facilities



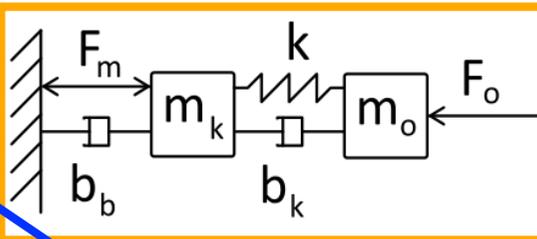


Facilities



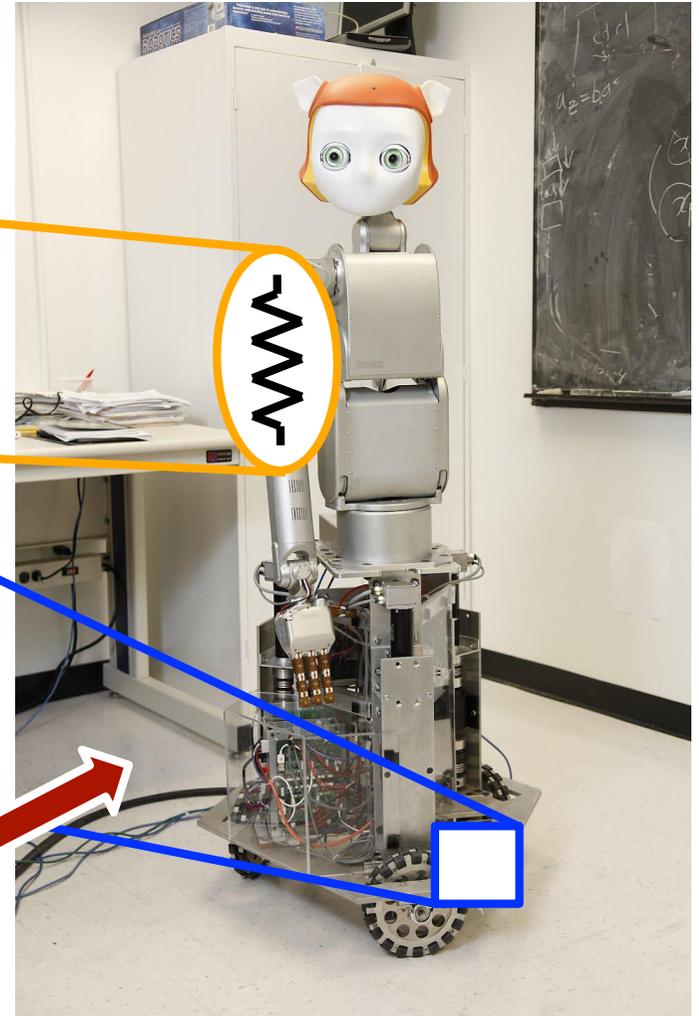


Facilities

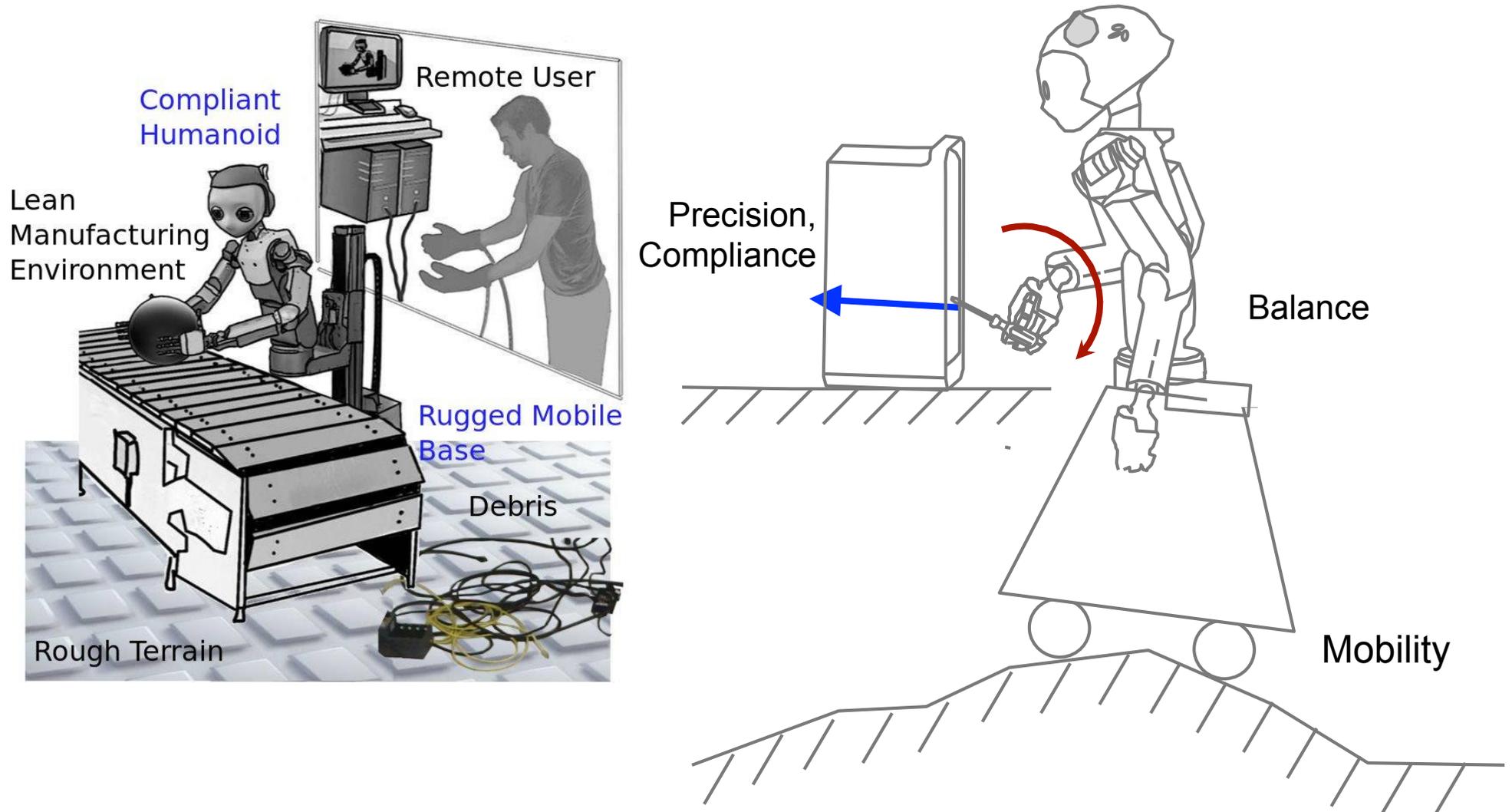


30 kg

120 kg

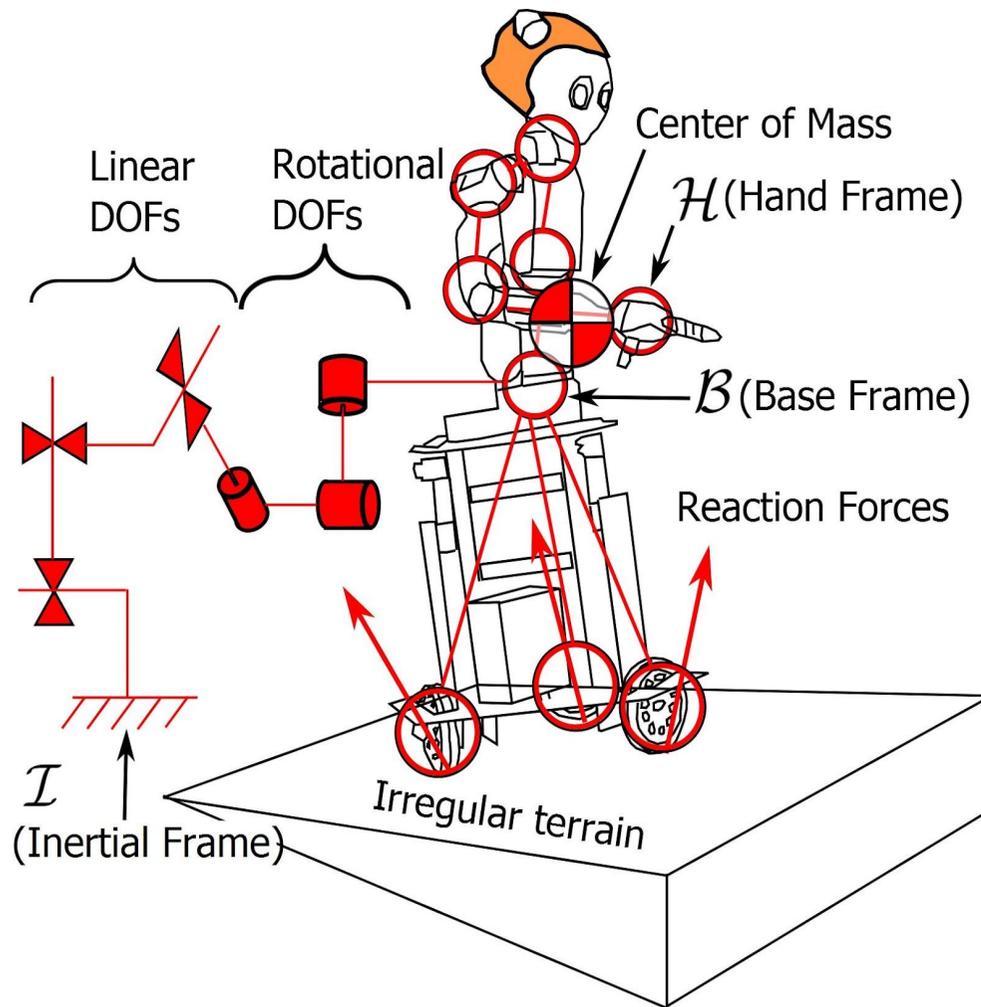


What is Rough Terrain Manipulation?



- Precisely manipulate the environment while adapting to terrain disturbances
- By precision tasks we mean hybrid position/force manipulation

Mechatronics of Dreamer



- 19 Degrees of Freedom
 - 10 DOFs torso/arm (hip coupled to trunk)
 - 3 DOFs holonomic base (triangle of omni wheels)
 - 6 unactuated (free-body dynamics)
- Various Constraints
 - omni wheels
 - supporting contact
 - biarticulate transmission
- Torque control
- Small footprint calls for balance
- Redundancy calls for posture control

Some Observations

Usually, base motions are treated as planar.

- unstated assumption: never lose contact
- "engineered-in" (broad & heavy base)
- but we need to handle contact changes!

Mobile manipulators rarely use balance.

- typically: broad & heavy base
- otherwise: planar assumption (e.g. Segways)

Objectives of the Research

Main Objective:

Understand rough terrain mobility; create operational space controllers; implement real-world demonstration on the rough terrains.

Sub Objectives:

- develop rough terrain constraints leading to holonomic base motion
- implement the required models for real-time control
- prove stability of posture control for the redundancies
- develop operational space balance control

Approach

Project the rigid body dynamics in a manifold that is consistent with internal/external constraints and underactuation.

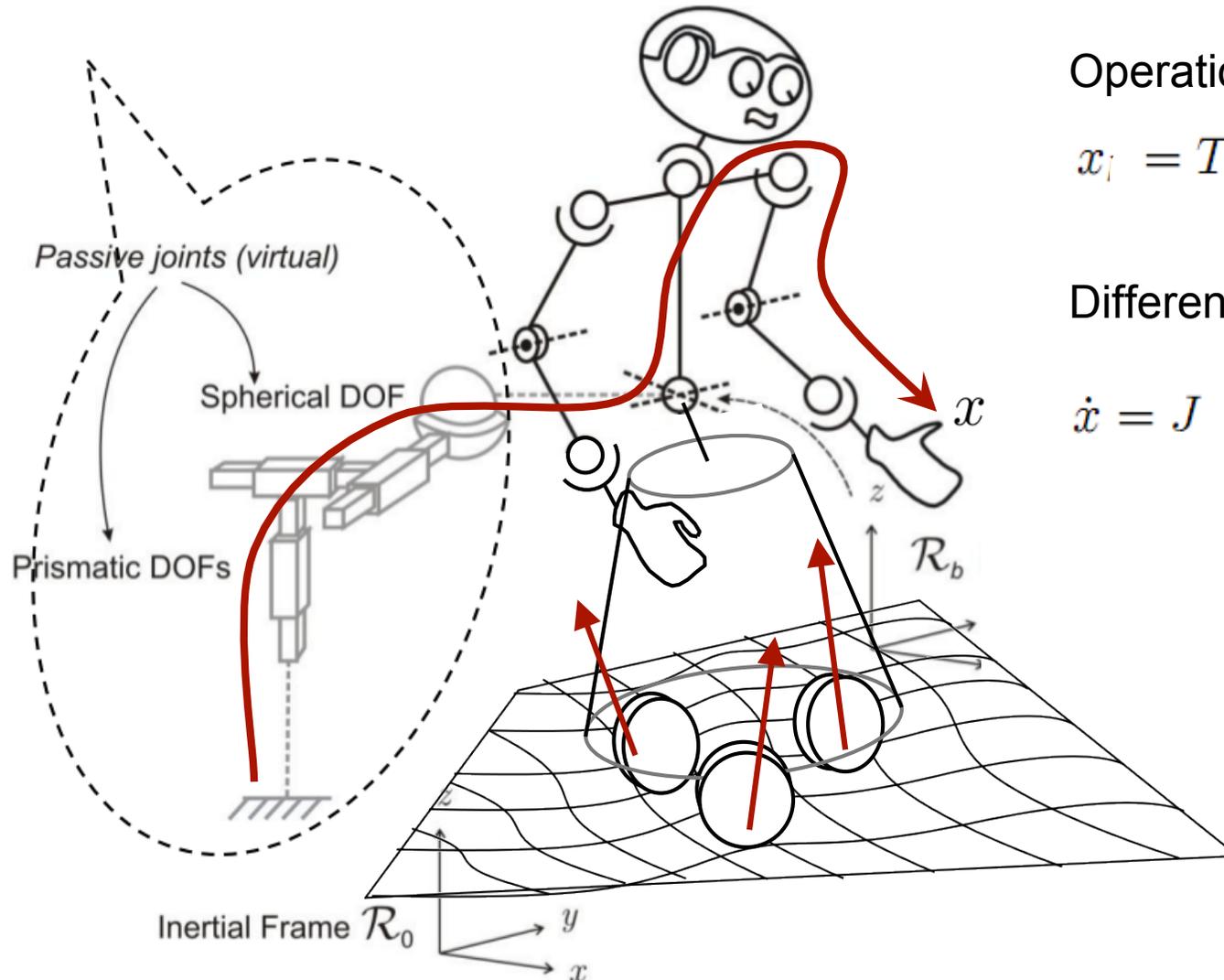
Develop operational space control for rough terrain systems; i.e. express constraints and underactuation via Generalized Jacobians.

Develop skills that can adapt to the environment and can be reused for various manipulation tasks.

Conduct experiments to validate each contribution.

Modeling **Constrained** Free Body Kinematics

(U) Underactuated DOFs



Operational Point (task joints)

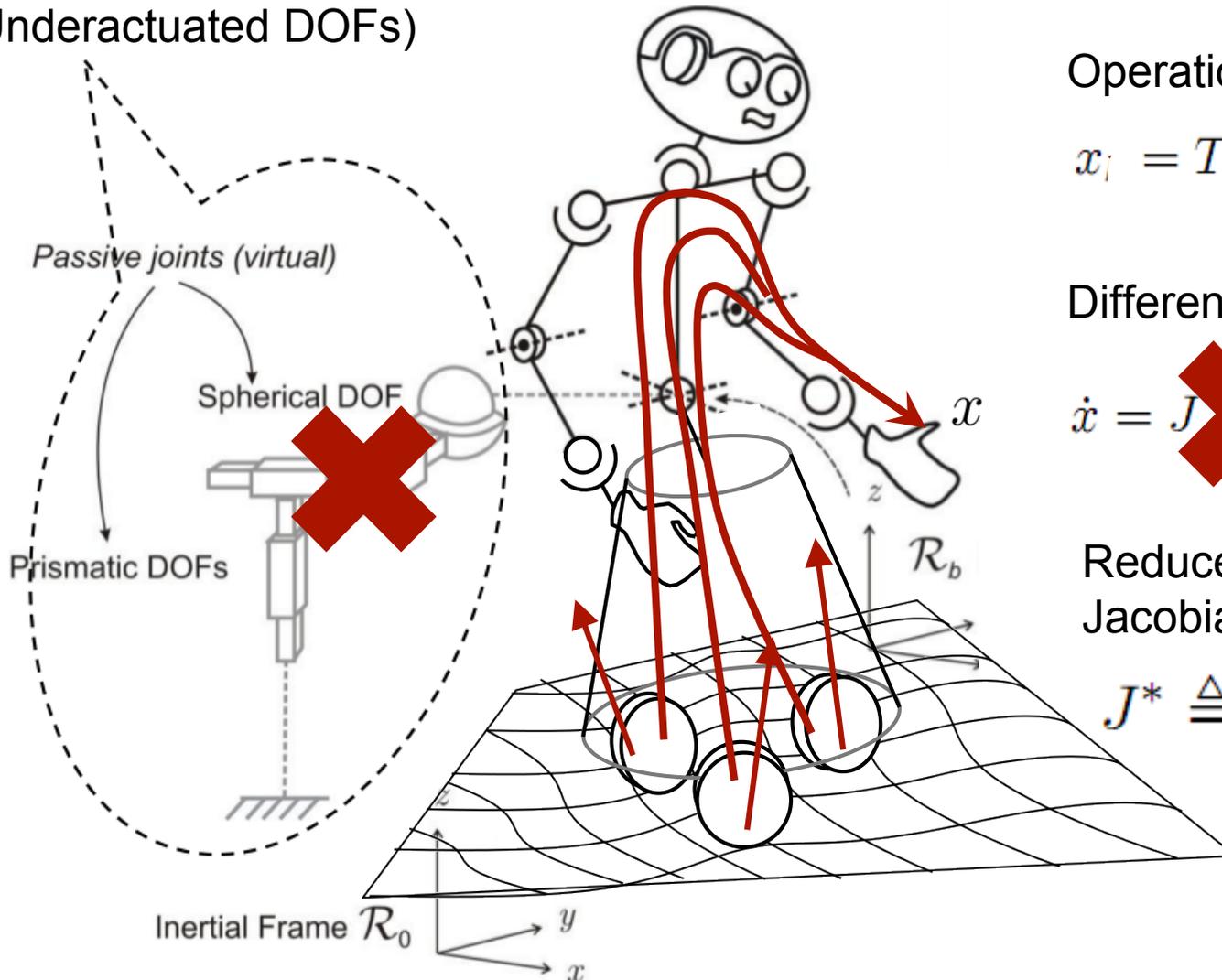
$$x_i = T[x_b, q]$$

Differential Kinematics

$$\dot{x} = J \begin{pmatrix} \dot{\vartheta}_b \\ \dot{q} \end{pmatrix}$$

Modeling **Constrained** Free Body Kinematics

(U) Non-holonomic Constraints
(Underactuated DOFs)



Operational Point (task joints)

$$x_i = T[x_b, q]$$

Differential Kinematics

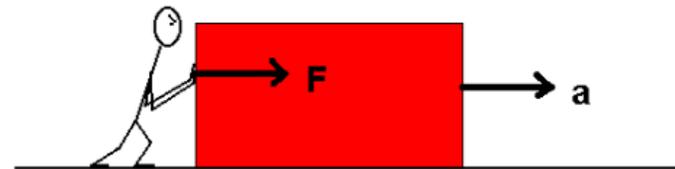
$$\dot{x} = J \left[\begin{matrix} \dot{x}_b \\ \dot{q} \end{matrix} \right] = J \overline{UN}_s \dot{q}$$

Reduced constraint consistent Jacobian

$$J^* \triangleq J \overline{UN}_s$$

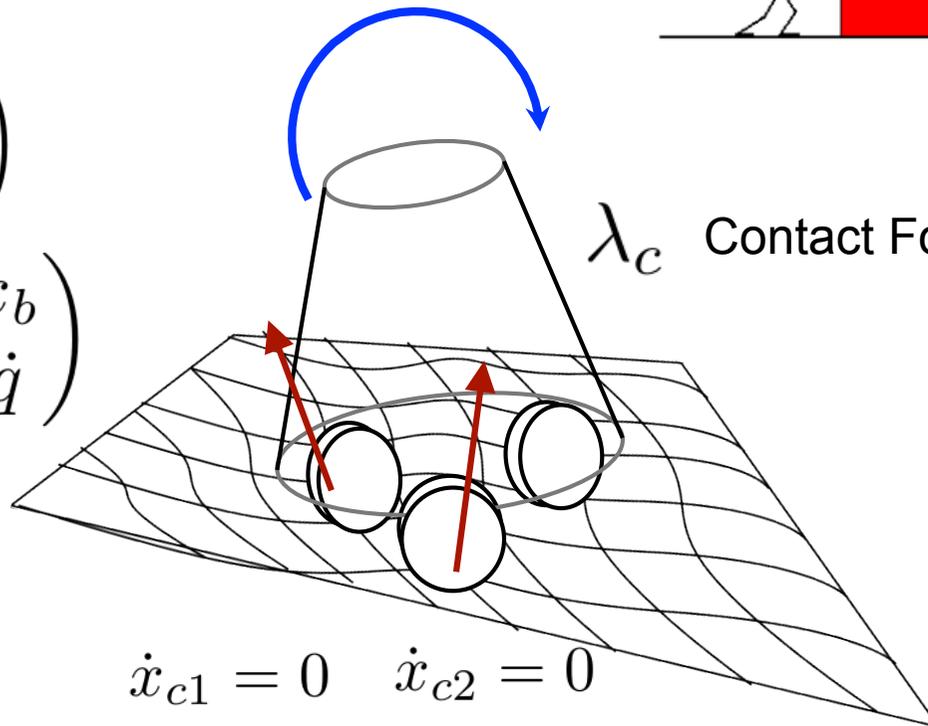
Incorporating Constraints on Dynamics

$$A \begin{pmatrix} \dot{v}_b \\ \ddot{q} \end{pmatrix} + B + G + J_c^T \lambda_c = \begin{pmatrix} 0_{6 \times 1} \\ \Gamma \end{pmatrix}$$



$$x_c = \begin{pmatrix} x_{c1} \\ x_{c2} \end{pmatrix}$$

$$\dot{x}_c = J_c \begin{pmatrix} \dot{x}_b \\ \dot{q} \end{pmatrix}$$

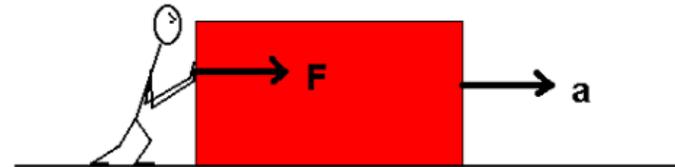


Base Mobility Constraints

Explicit solution

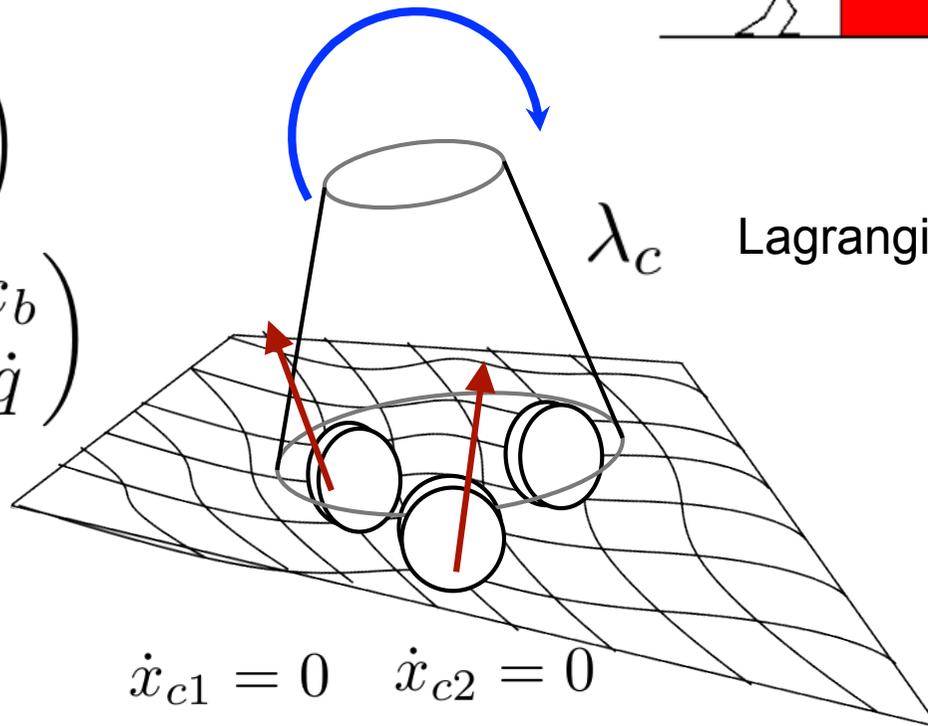
$$\lambda_c = \bar{J}_c^T (U^T \Gamma - B - G) + \Lambda_c \dot{J}_c \begin{pmatrix} \dot{x}_b \\ \dot{q} \end{pmatrix}$$

$$A \begin{pmatrix} \dot{\vartheta}_b \\ \dot{q} \end{pmatrix} + B + G + J_c^T \lambda_c = \begin{pmatrix} 0_{6 \times 1} \\ \Gamma \end{pmatrix}$$



$$x_c = \begin{pmatrix} x_{c1} \\ x_{c2} \end{pmatrix}$$

$$\dot{x}_c = J_c \begin{pmatrix} \dot{x}_b \\ \dot{q} \end{pmatrix}$$



λ_c Lagrangian multipliers

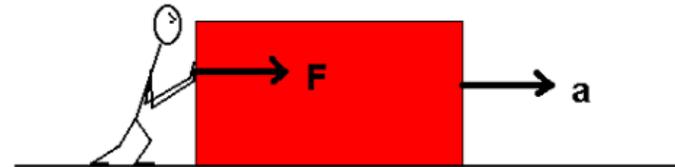
$$\dot{x}_{c1} = 0 \quad \dot{x}_{c2} = 0$$

Base Mobility Constraints

Implicit solution

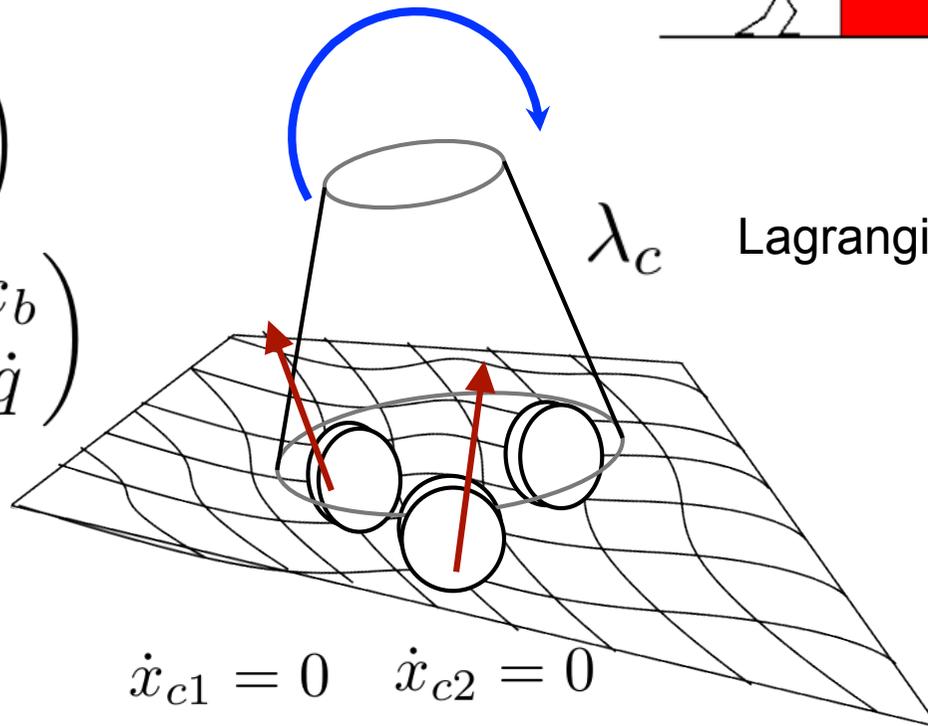
$$A \begin{pmatrix} \dot{\vartheta}_b \\ \ddot{q} \end{pmatrix} + N_c^T (B + G) + J_c^T \Lambda_c \dot{J}_c \begin{pmatrix} \vartheta_b \\ \dot{q} \end{pmatrix} = (U N_c)^T \Gamma$$

$$\lambda_c = \bar{J}_c^T (U^T \Gamma - B - G) + \Lambda_c \dot{J}_c \begin{pmatrix} \dot{x}_b \\ \dot{q} \end{pmatrix}$$



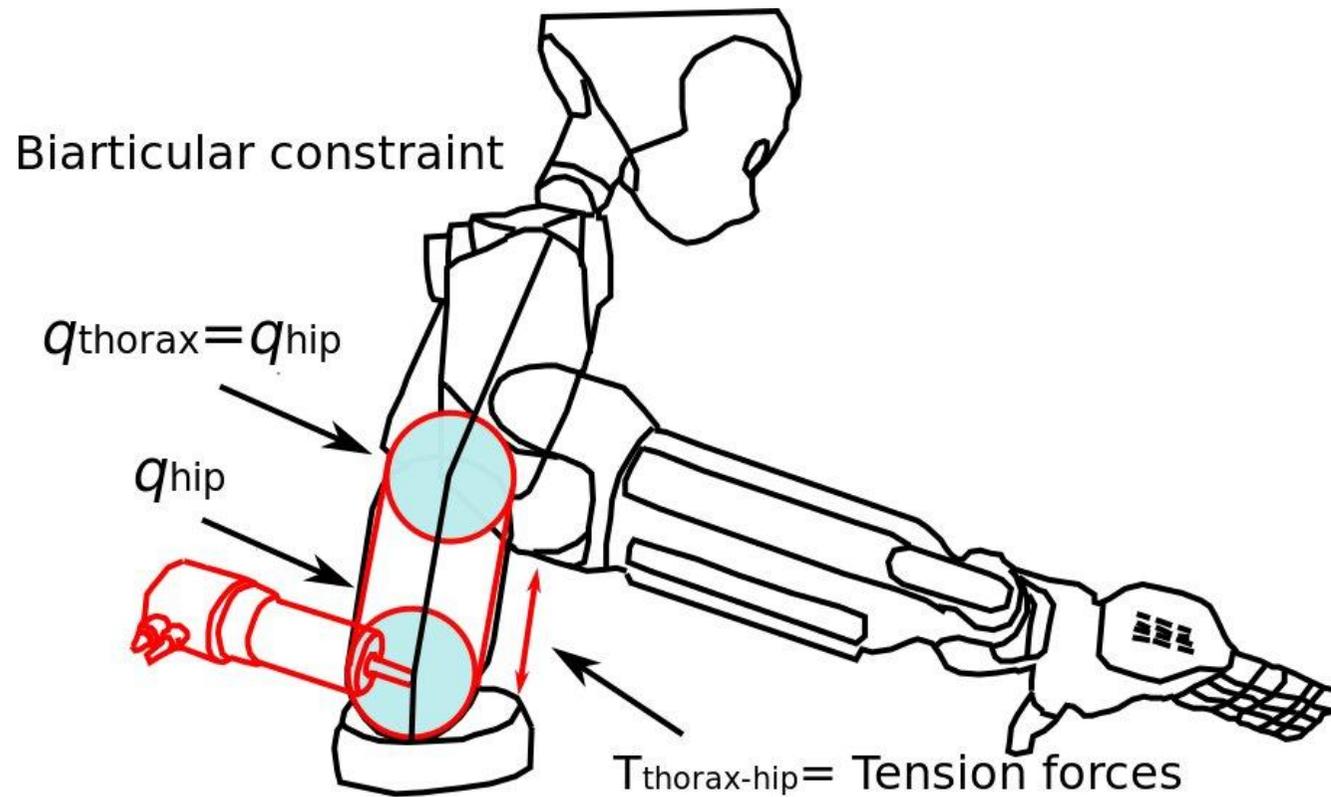
$$x_c = \begin{pmatrix} x_{c1} \\ x_{c2} \end{pmatrix}$$

$$\dot{x}_c = J_c \begin{pmatrix} \dot{x}_b \\ \dot{q} \end{pmatrix}$$



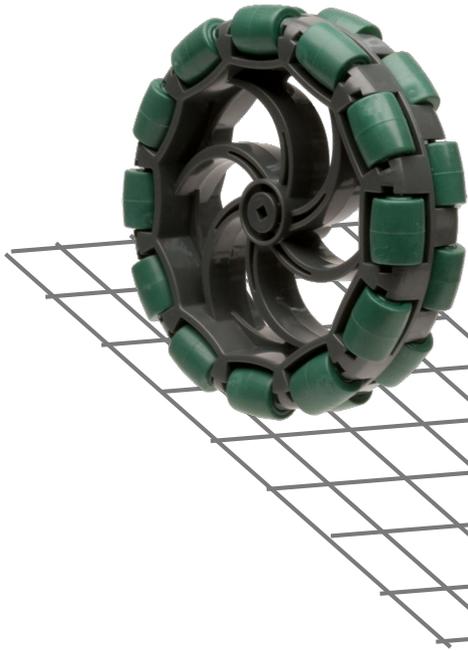
λ_c Lagrangian multipliers

Biarticular Transmission Constraints



$$J_{\text{biart}} \triangleq \left([0]_{1 \times 6} \ [0]_{1 \times 3} \ 0 \ 1 \ -1 \ [0]_{1 \times 7} \right) \in \mathbb{R}^{1 \times n_{\text{dofs}}}$$

Rolling Constraints (immobile contact)

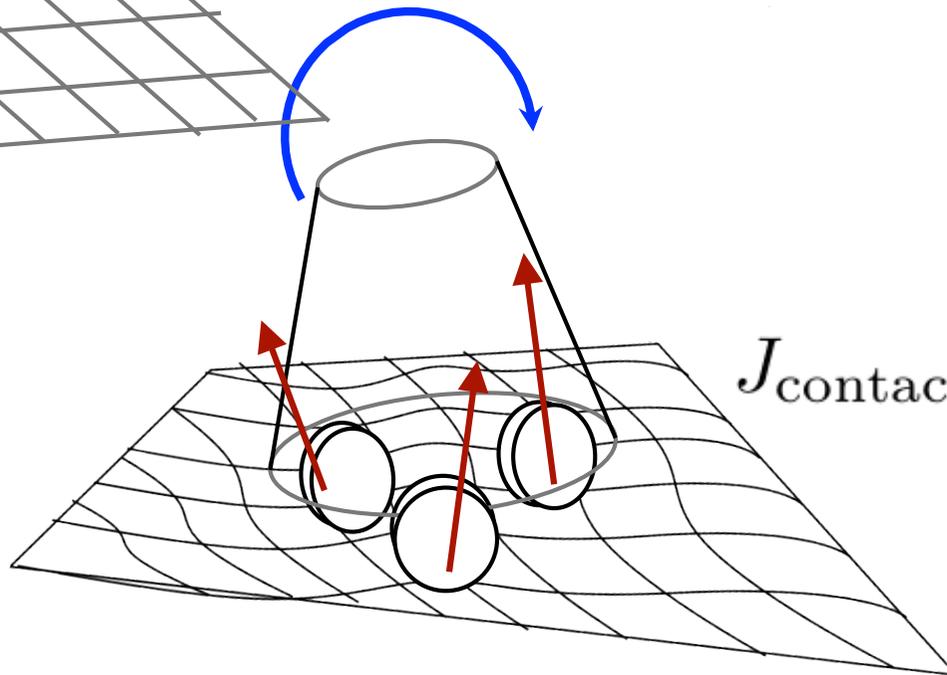


$$v_{\text{contact}[i]} = v_{\text{wheel}[i]} + \omega_{\text{wheel}[i]} \times \delta_{\text{contact}[i]} \in \mathbb{R}^3$$

$$u_{\text{rolling}[i]}^T v_{\text{contact}[i]} = 0$$

$$J_{\text{rolling}[i]} \triangleq u_{\text{rolling}[i]}^T \left(J_{v,\text{wheel}[i]} - \delta_{\text{contact}[i]} \times J_{\omega,\text{wheel}[i]} \right)$$

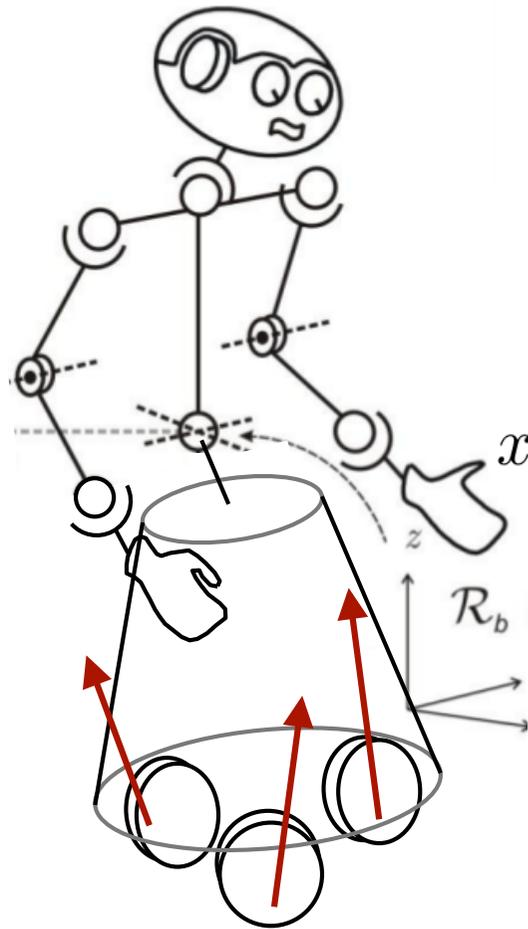
$$J_{\text{normal}[i]} \triangleq u_{\text{normal}[i]}^T J_{\text{wheel}}$$



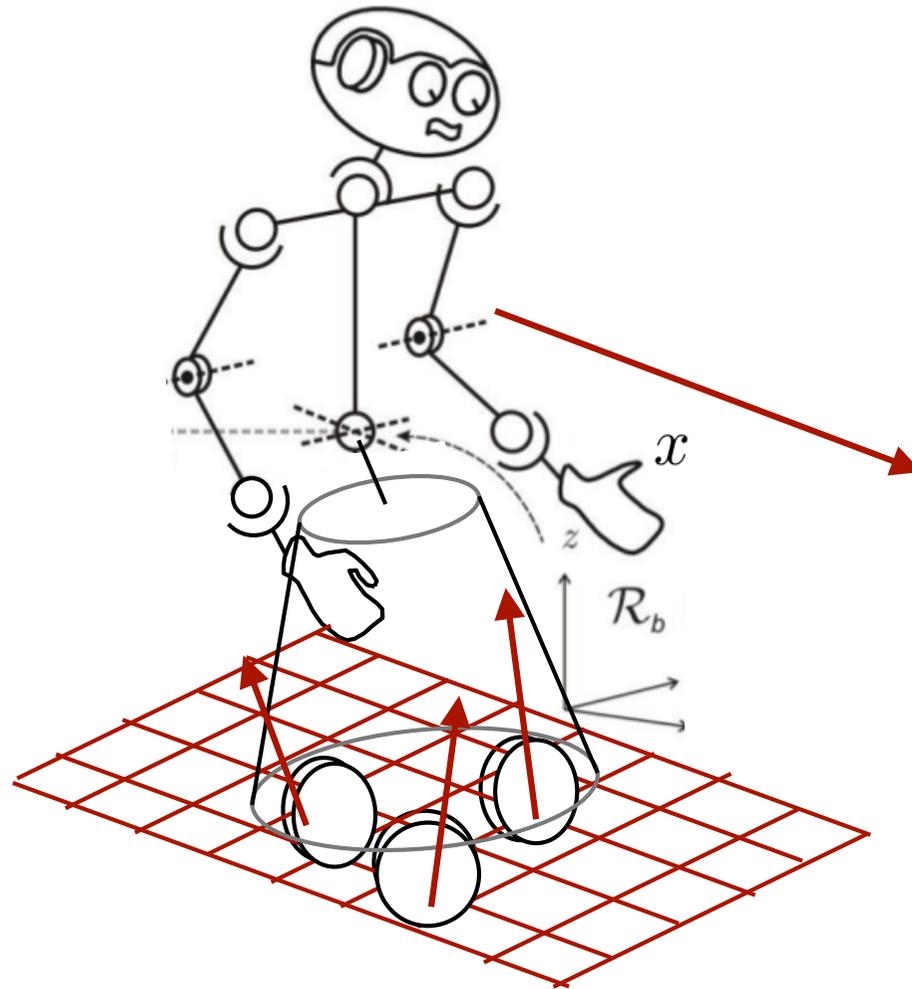
$J_{\text{contact}} \triangleq$

$$\begin{pmatrix} J_{\text{rolling}[1]} \\ J_{\text{rolling}[2]} \\ J_{\text{rolling}[3]} \\ J_{\text{normal}[1]} \\ J_{\text{normal}[2]} \\ J_{\text{normal}[3]} \end{pmatrix} \in \mathbb{R}^6$$

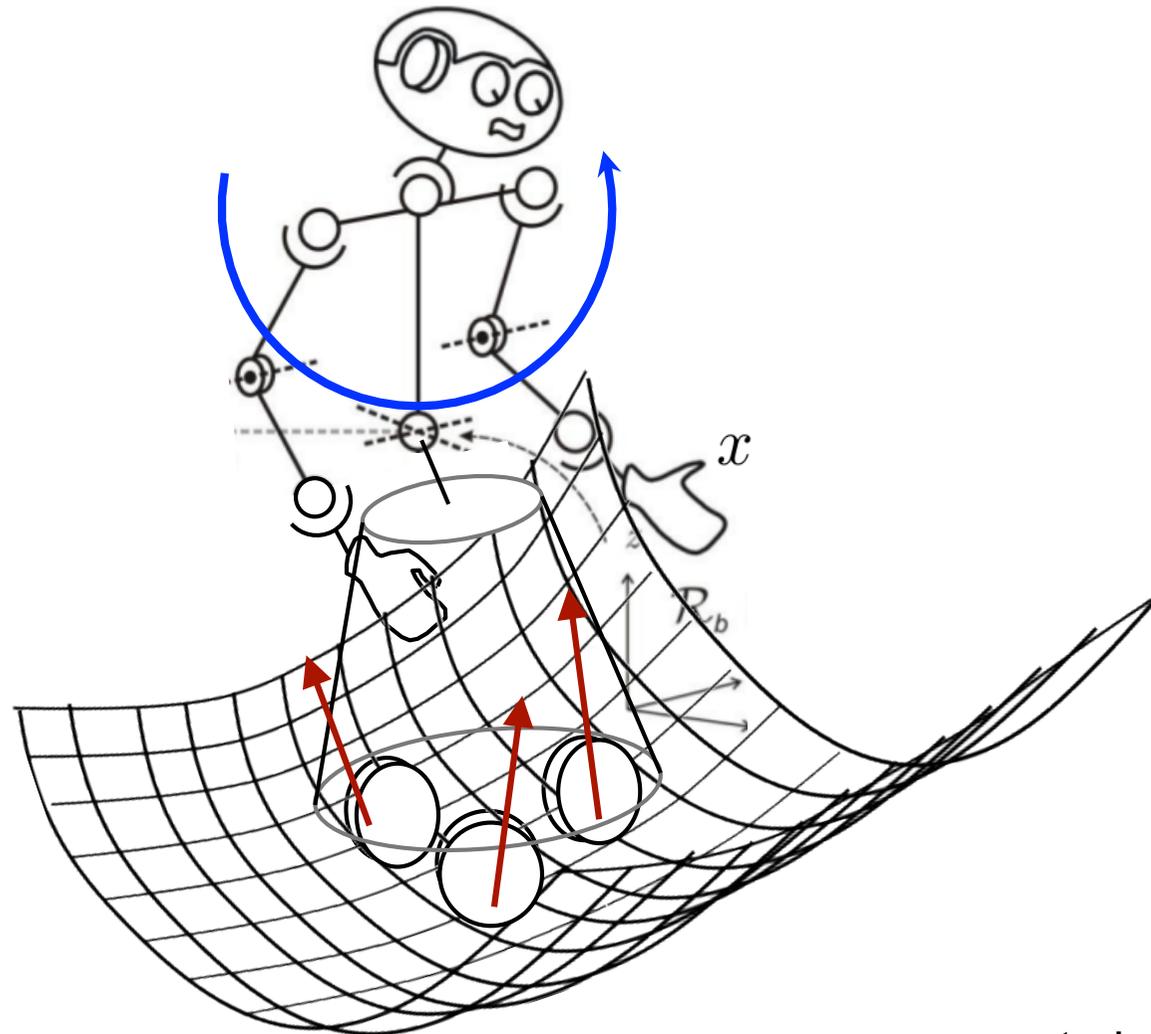
Analysis of Holonomic Motion



Analysis of Holonomic Motion

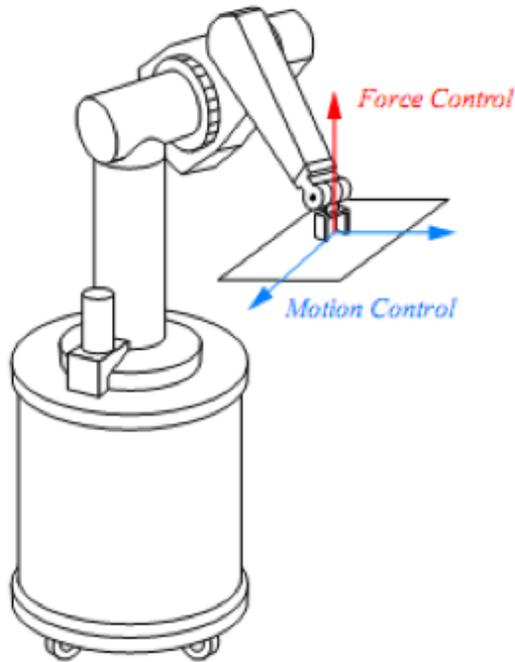


Analysis of Holonomic Motion



...to be studied further...

Operational Space Control



Stanford robotics / AI lab

Control of the task forces (pple virtual work)

$$\Gamma = J_{\text{task}}^T F_{\text{task}}$$

Impedance control of task motion

$$F_{\text{task}} = \Lambda_{\text{task}} a_{\text{des}} + \mu_{\text{task}} + p_{\text{task}}$$

Linear Control



$$\ddot{x}_{\text{task}} = a_{\text{des}}$$

Potential Fields



$$a_{\text{des}} = -K_p \nabla V_{\text{task}} - K_v \dot{x}_{\text{task}}$$

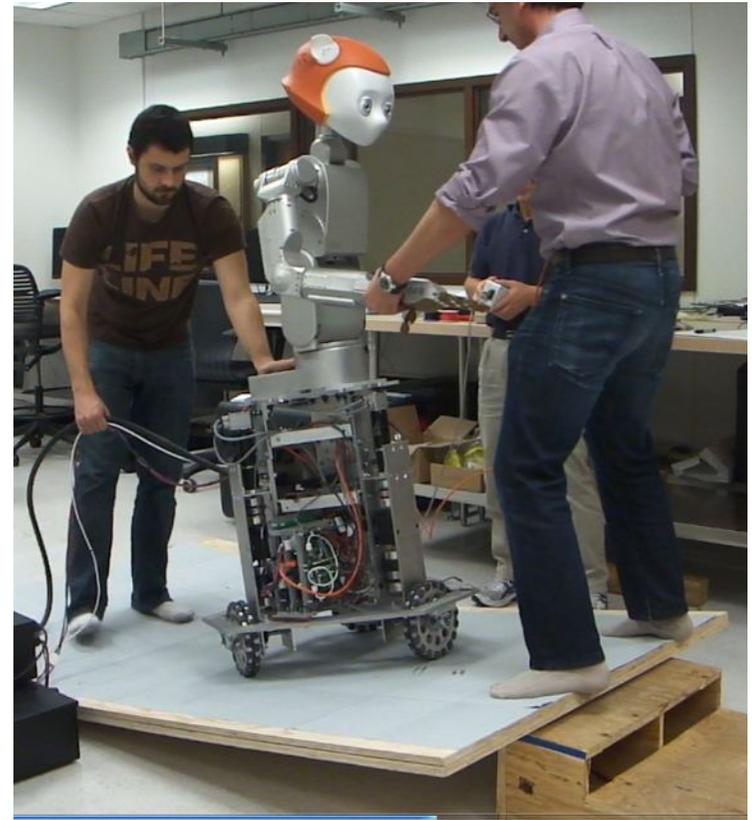


Operational Space Control on Rough Terrains



[Khatib ca 1998]

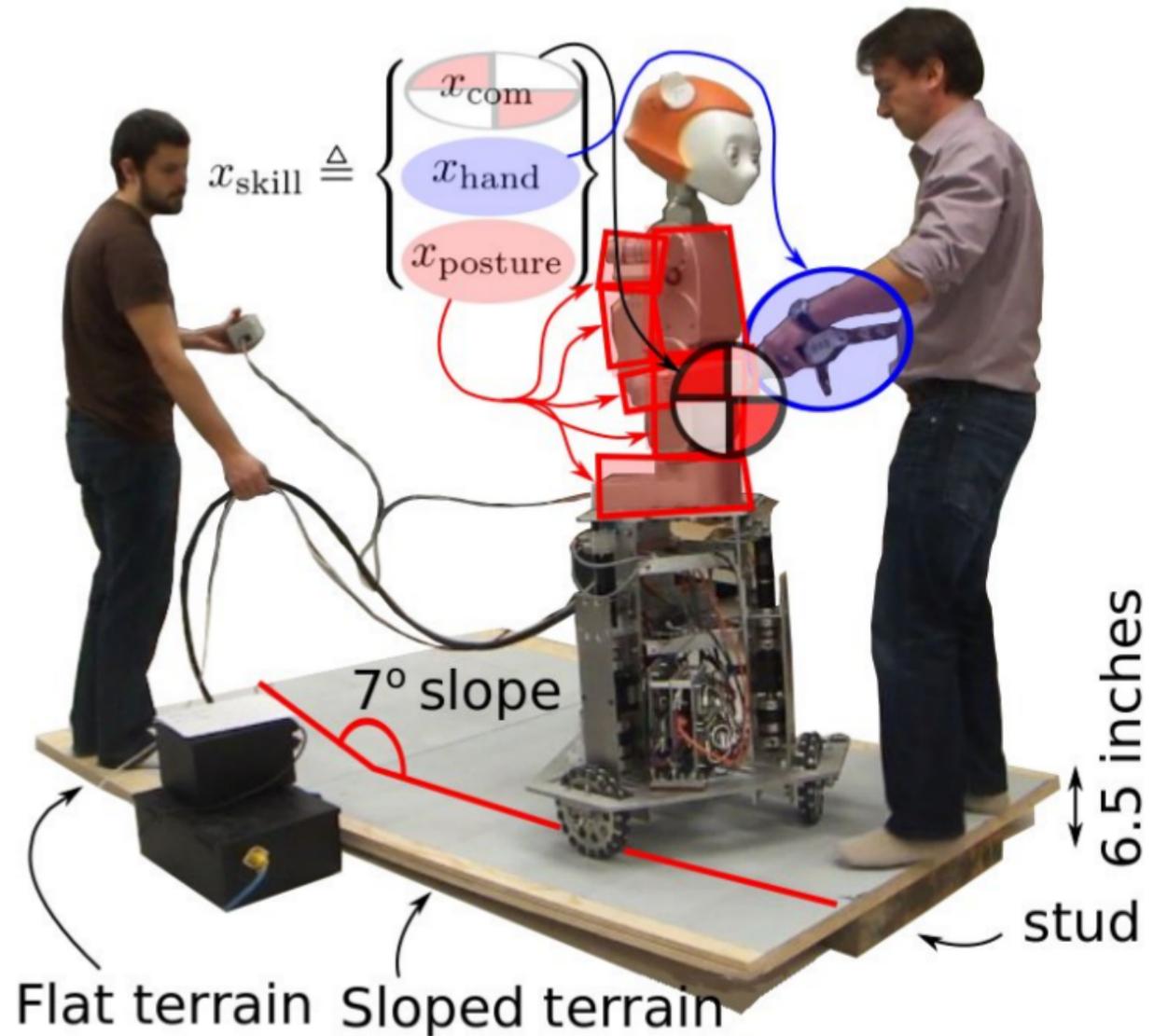
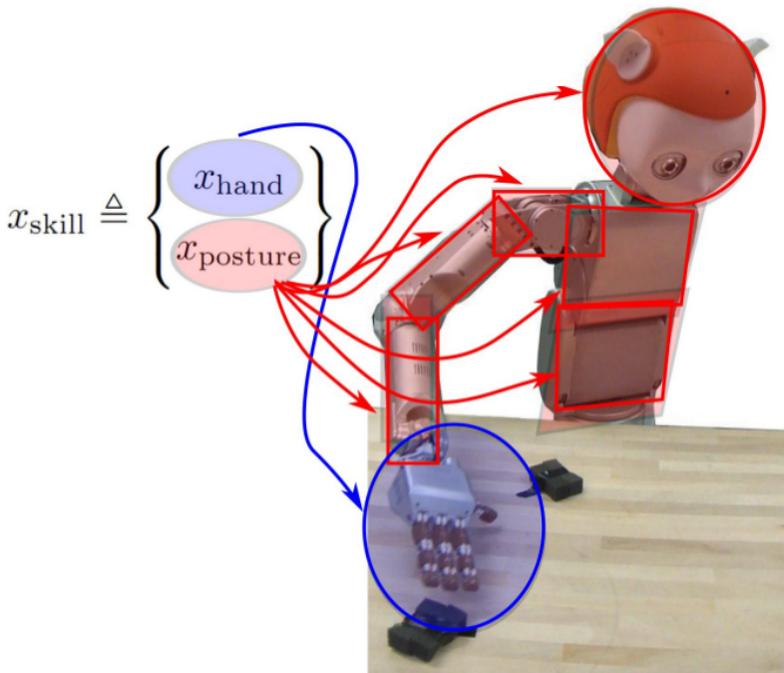
$$\Gamma = J^T F + N^T \Gamma_p$$



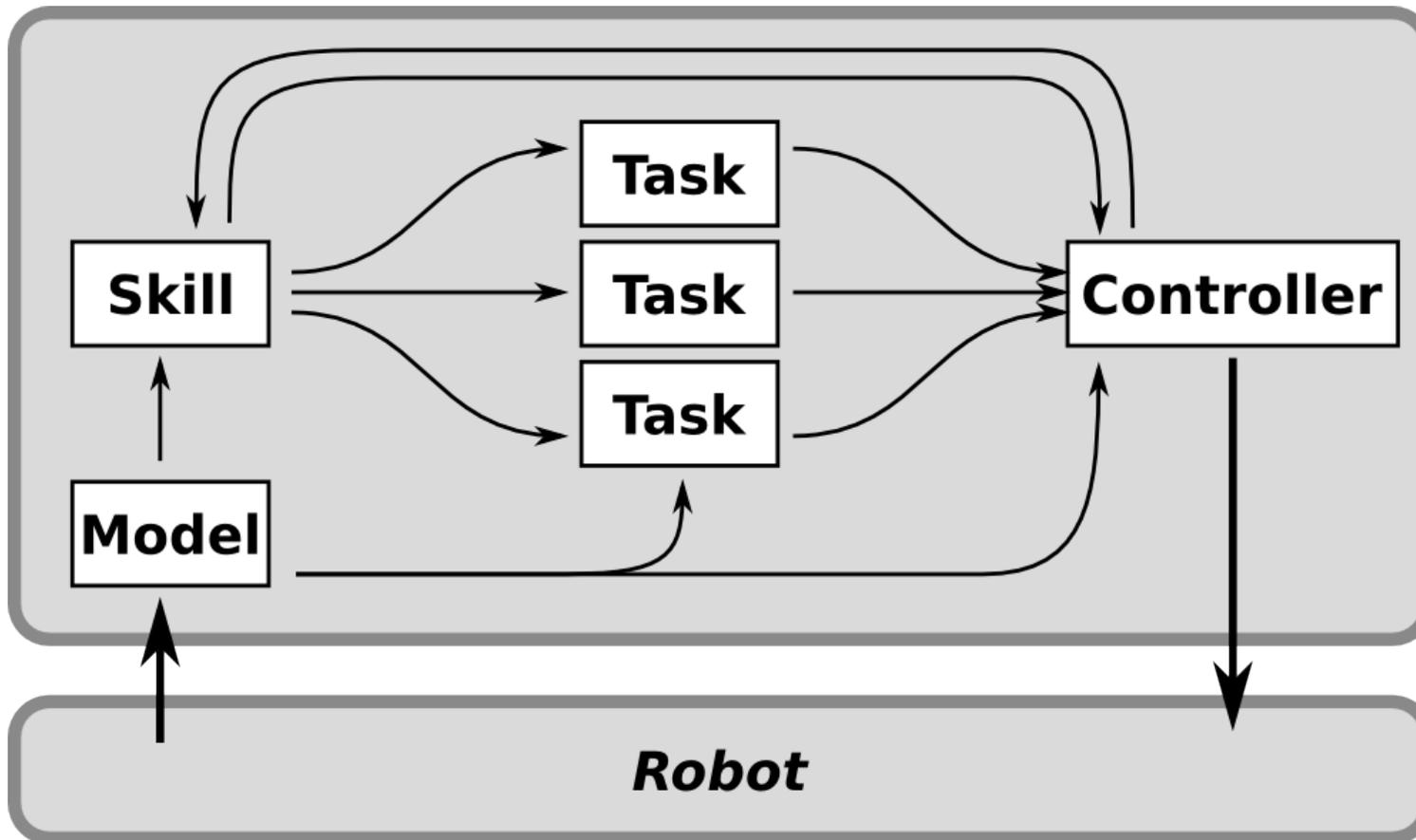
$$\Gamma = J^{*T} F + N^{*T} \Gamma_p$$

Can be generalized to any number of “**tasks**”...

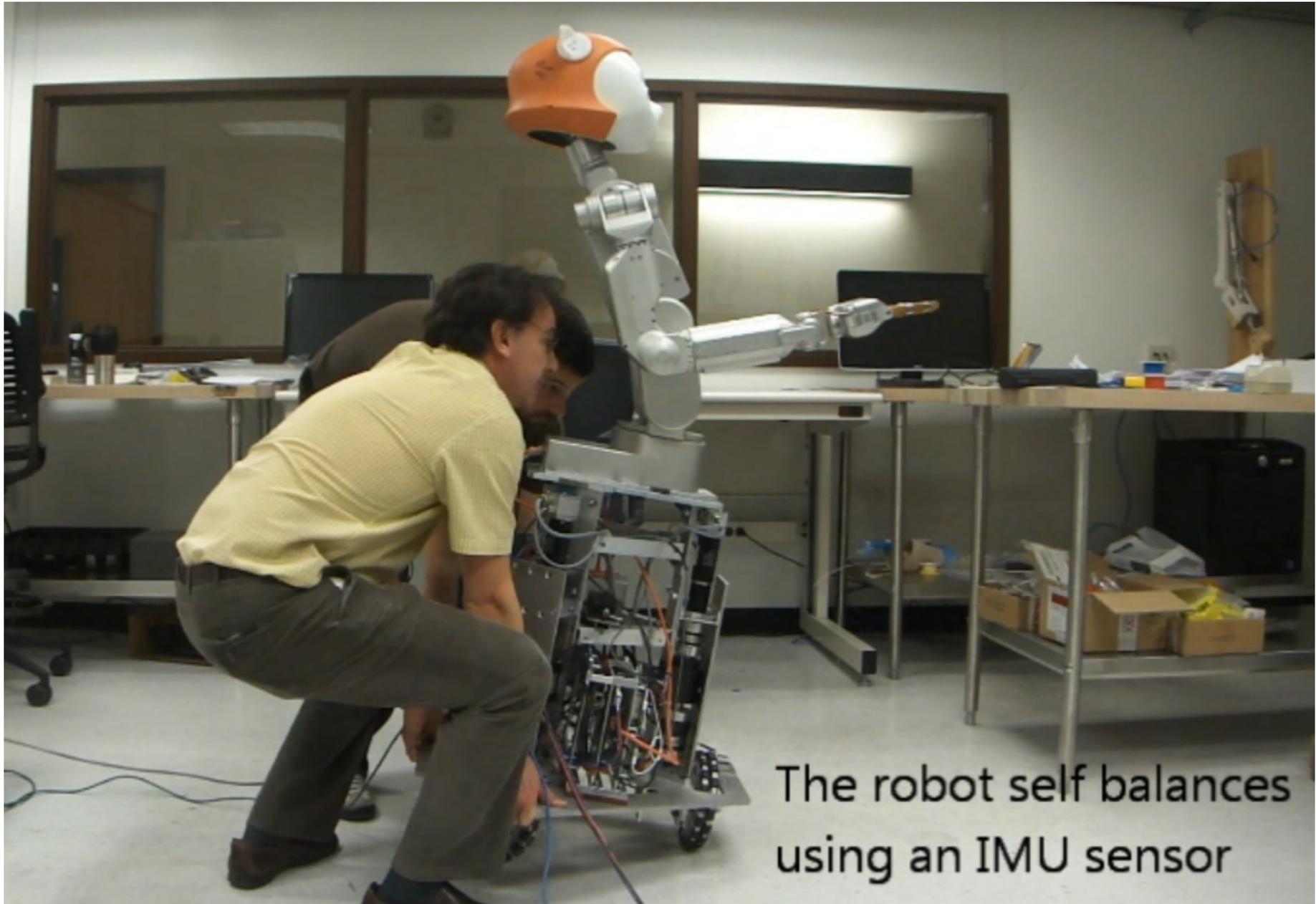
Skills for Experiments with Dreamer



Software Architecture

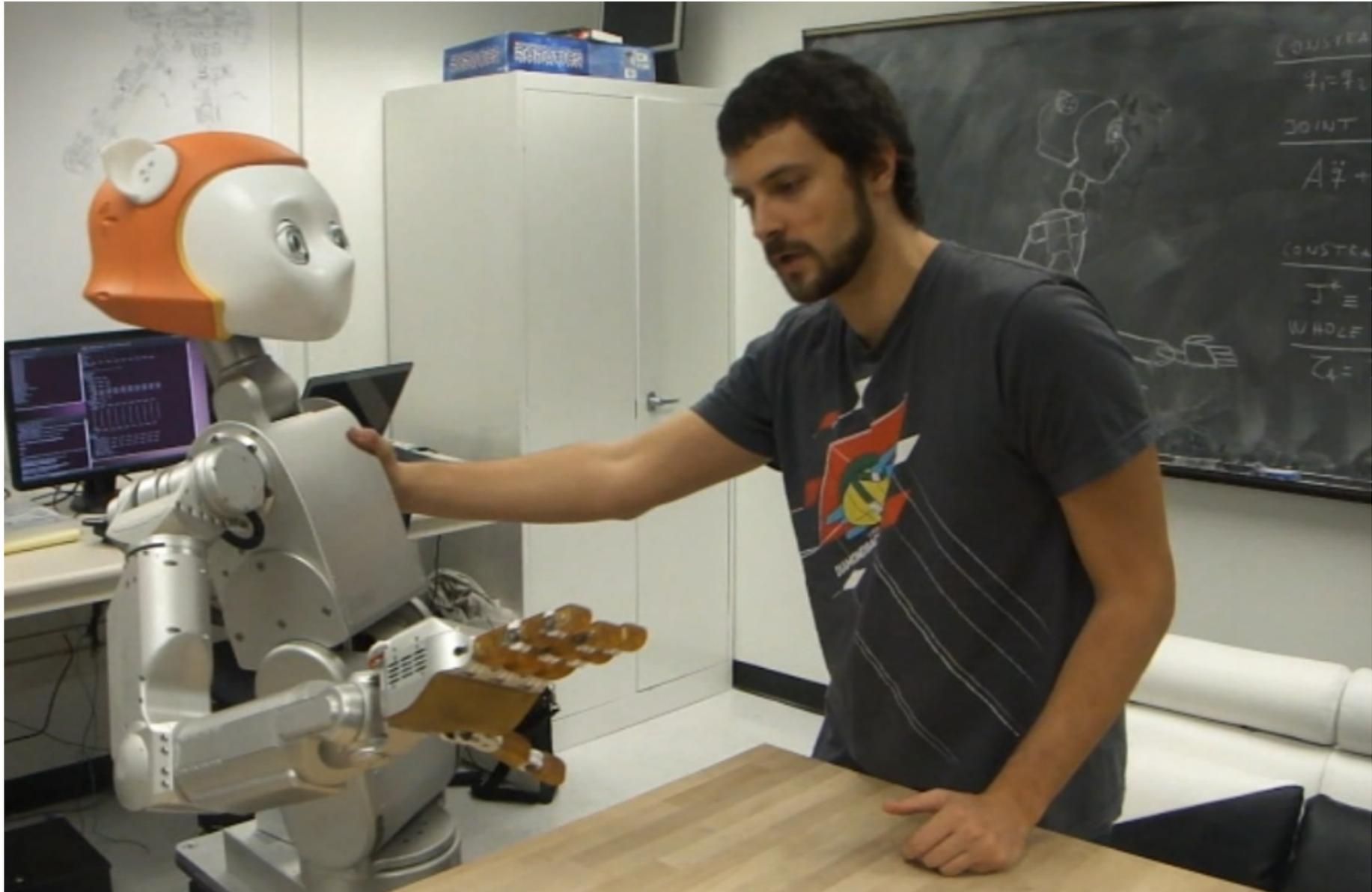


Experiment 1: Balancing

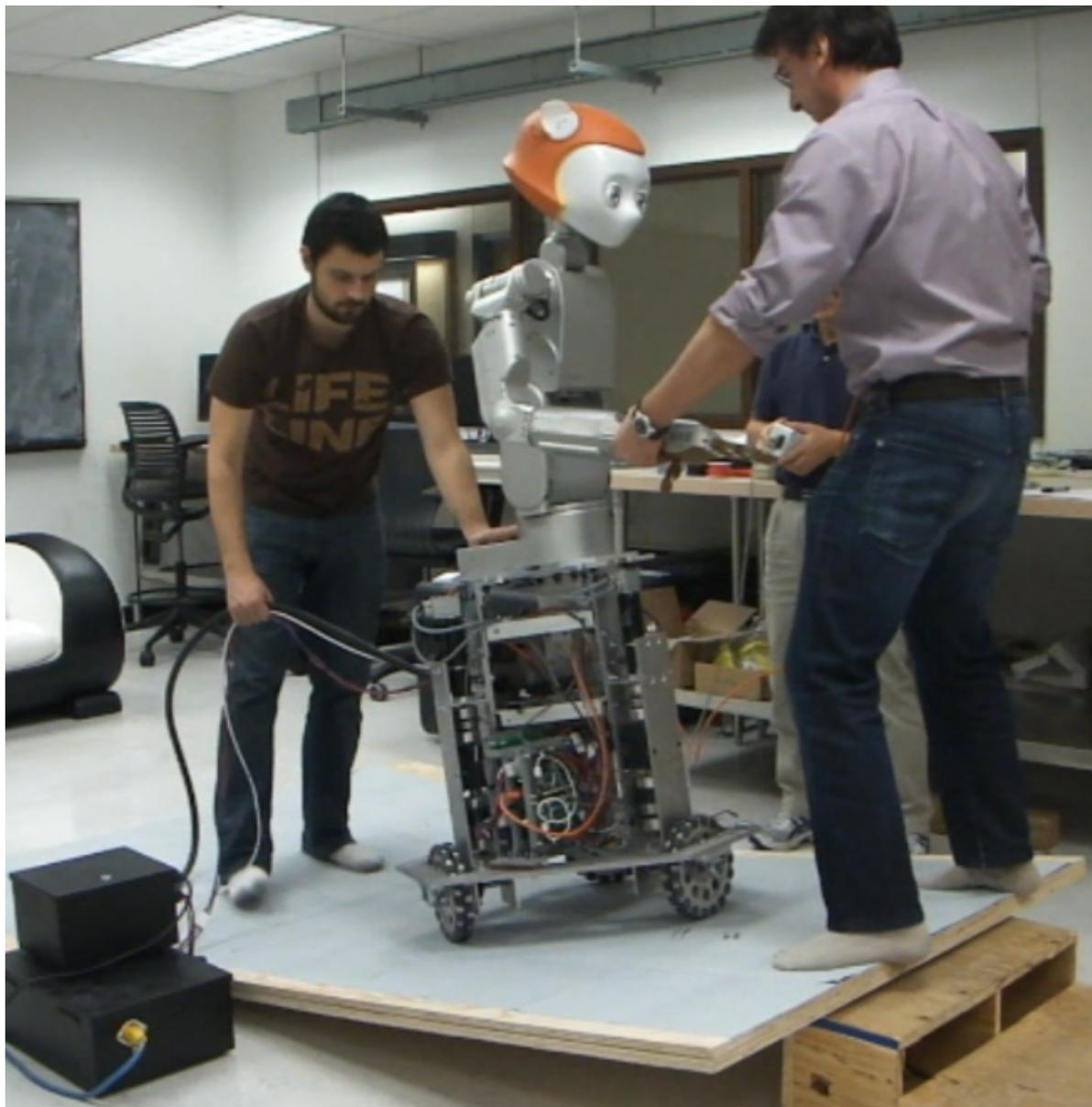


The robot self balances using an IMU sensor

Experiment 2: Reaching



Experiment 3: Rough Terrain Kinesthetic Interaction



Conclusions

- Rough terrain manipulation will allow mobile humanoids to work...
 - + outdoors
 - + in flexible manufacturing
 - + in houses, *etc*
- We need models that characterize the roughness of the terrain.
 - + new interpretation of holonomic mobility
- Operational space whole-body control can be easily extended to provide compliant control for mobile manipulation in rough terrains.
- Real-time capability for 19 DOF robot using off-the-shelf PC

Outlook

- changing contact
- dynamic balance
- study conditions for holonomicities
- build a collection of reusable skills

Thank You!