Channel Estimation and Compensation in Chromatic Dispersion Limited Optical Fast OFDM Systems

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Abstract— We experimentally investigate the channel estimation and compensation in a chromatic dispersion (CD) limited 20Gbit/s optical fast orthogonal frequency division multiplexing (F-OFDM) system with up to 840km transmission. It is shown that symmetric extension based guard interval (GI) is required to enable CD compensation using one-tap equalizers. As few as one optical F-OFDM symbol with four and six pilot tones per symbol can achieve near-optimal channel estimation and compensation performance for 600km and 840km respectively.

I. INTRODUCTION

Optical fast orthogonal frequency division multiplexing (F-OFDM) [1-5], with sub-channel spacing equal to half of that in conventional OFDM, is a promising multi-carrier scheme. The sub-carrier multiplexing/demultiplexing can be implemented by using the inverse discrete cosine transform (IDCT)/DCT. The excellent energy concentration property of DCT results in the enhanced robustness to frequency offset [6] and improved performance in channel estimation [7] when compared to conventional OFDM [8, 9]. Furthermore, the DCT, which has been widely adopted in image standards, uses only real arithmetic in contrast to the discrete Fourier transform (DFT) in conventional optical OFDM, whose output is complex even when the input is real. This not only reduces the implementation cost for cost-sensitive applications, but also increases resilience to in-phase/quadrature imbalance.

Due to the different properties of DFT and DCT, the techniques of conventional OFDM cannot be simply employed for F-OFDM and it is necessary to implement solutions specific to optical F-OFDM. In particular, the diagonalizing property of DFT for a circulant channel matrix is not applicable to DCT, such that cyclic prefix (CP) based guard interval (GI) cannot enable ideal chromatic dispersion (CD) compensation using one-tap equalizers. One solution is to use frequency or time domain equalization before channel demultiplexing [3-4], which however increases the implementation complexity. Extending the whole data sequence can enable CD compensation using one-tap equalizers [10-11], but reduces the information throughput by a factor of two. In wireless, other methods such as zero padding [6] or front-end pre-filtering [12] have been used to mitigate fading effects. In [5], it has been shown that the CD-induced channel matrix can be diagonalized by DCT when symmetric extension (SE) based GI is used, enabling CD to be compensated using one-tap equalizers after DCT without any pre-filtering. In this paper, we will experimentally characterize the channel estimation and compensation in a CD-limited 20Gbit/s optical F-OFDM system based on double-side band four-level amplitude shifted keying (4-ASK) sub-carrier modulation with transmission up to 840km. It is confirmed that SE-based rather than CP-based GI is required to enable CD compensation using one-tap equalizers. As few as one F-OFDM symbol with six pilot tones per symbol can achieve near-optimal channel estimation and compensation performance for 840km transmission.

II. EXPERIMENTAL SETUP

![Fig. 1. Experimental setup of 20Gbit/s 4-ASK optical F-OFDM.](image)

![Fig. 2. Cyclic and symmetric extension based guard interval.](image)
Fig. 1 shows the experimental setup. The bi-polar 4-ASK based F-OFDM signal was encoded with gray code in Matlab. The inverse-DCT (IDCT) and DCT used 256 points, of which 213 sub-carriers (sub-carriers #2–#214) were used for data transmission. The first sub-carrier (DC) was not modulated, allowing for AC-coupled driving amplifiers and receivers. After IDCT and parallel-to-serial (P/S) conversion, 0, 2, 6, or 12 samples were added to each symbol as a SE based GI, whose principle is depicted in Fig. 2. By using the SE-based GI, the CD-induced channel matrix could be represented as the sum of a symmetric Toeplitz matrix and a Hankel matrix [5], which could be diagonalized by DCT/IDCT [12]. Consequently, at the receiver, each F-OFDM symbol could be demultiplexed by DCT without inter-carrier interference and CD only resulted in different constants multiplied to different sub-carrier data. For comparison, CP based GI with 12 samples was also investigated.

The generated F-OFDM signal was downloaded to a 12GS/s arbitrary waveform generator (AWG) with a resolution of 8 bits. The nominal symbol rate including the GI, forward error correction overhead, etc was 10Gsym/s (12×213/256). The inset of Fig. 1 depicts the electrical spectrum after the AWG, where the electrical bandwidth for 20Gbit/s 4-ASK F-OFDM signal was 5GHz due to the reduced sub-channel spacing equal to half of the symbol rate per sub-carrier. The frequency components beyond 5GHz were due to aliasing. A fibre laser with 6kHz linewidth was used to generate the optical carrier. A Mach-Zehnder modulator (MZM) was used for signal modulation with a peak-to-peak signal input voltage of around 0.5Vπ. The modulated optical signal was then amplified by an erbium doped fibre amplifier (EDFA), filtered by a 0.8nm optical band-pass filter (OBPF), and transmitted over a recirculating loop comprising 60km single-mode fibre (SMF) with 13dB fibre loss. The noise figure of the loop EDFA was 5dB and another 0.8nm OBPF was used in the loop to suppress the amplified spontaneous emission noise. The launch power was set to be -4.5dBm using a variable optical attenuator (VOA).

At the receiver, the optical signal was detected with a pre-amplified coherent receiver and a VOA was used to vary the optical signal-to-noise ratio (OSNR). The pre-amplifier was followed by an OBPF with a 3dB bandwidth of 0.3nm, a second EDFA, and another optical filter with a 3dB bandwidth of 1nm. A polarization controller (PC) was used to align the polarization of the filtered F-OFDM signal before entering the signal path of a 90° optical hybrid. A tap of the transmitter laser signal filtered F-OFDM signal before entering the signal path of the controller (PC) was used to align the polarization of the filter with a 3dB bandwidth of 1nm. A polarization bandwidth of 0.3nm, a second EDFA, and another optical amplifier was followed by an OBPF with a 3dB bandwidth of 1nm used to vary the optical signal-to-noise ratio (OSNR). The pre-amplified coherent receiver and a VOA was used to vary the optical signal-to-noise ratio (OSNR). The pre-amplified coherent receiver and a VOA was used to vary the optical signal-to-noise ratio (OSNR). The pre-amplified coherent receiver and a VOA was used to vary the optical signal-to-noise ratio (OSNR). The pre-amplified coherent receiver and a VOA was used to vary the optical signal-to-noise ratio (OSNR).

The noise figure of the loop EDFA was 5dB due to cascaded filtering in the loop, and de-polarization during transmission.

### III. RESULTS AND DISCUSSIONS

Fig. 3 depicts the performance of 4-ASK optical F-OFDM using SE-based GI (solid symbols) after 600km and 840km, in comparison with CP-based GI (empty symbols). It is shown that when CP-based GI is used, the performance is significantly degraded and BER of 10⁻³ cannot be achieved even using a GI length of 12 at ~17dB OSNR. In contrast, SE-based GI results in better performance, and the required OSNRs to achieve BER of 10⁻³ for 600km and 840km are around 13dB. The slight penalty for the 840km case with respect to the 600km case may have been caused by fibre nonlinearity [5], the effect of cascaded filtering in the loop, and de-polarization during transmission.

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**Fig. 3.** Performance versus received OSNR for different SE-based GI lengths at 600km and 840km, in comparison with CP-based GI (empty symbols). It is shown that when CP-based GI is used, the performance is significantly degraded and BER of 10⁻³ cannot be achieved even using a GI length of 12 at ~17dB OSNR. In contrast, SE-based GI results in better performance, and the required OSNRs to achieve BER of 10⁻³ for 600km and 840km are around 13dB. The slight penalty for the 840km case with respect to the 600km case may have been caused by fibre nonlinearity [5], the effect of cascaded filtering in the loop, and de-polarization during transmission.

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**Fig. 4.** Performance versus received OSNR for different SE-based GI lengths at 840km. Channel estimation is obtained using all data sub-carriers as pilot tones in 20 training symbols.
To characterize the relation between the transmission performance and the GI length, Fig. 4 shows BER versus received OSNR for different SE-based GI lengths at 840km. It is straightforwardly observed that a longer GI length results in better performance. This conclusion is further confirmed by Fig. 5, where BER versus fibre length for different GI lengths at -34dBm is depicted. Note that at -34dBm received power, the OSNR values are different at different fibre lengths, varying from 17.9dB for 120km to 17.1dB for 840km. When compared to a GI length of 12, the case without GI results in degraded performance even at 240km. The use of 2-sample GI length ensures small penalties up to 360km, after which, however, the BER is degraded severely. Further increasing the GI length to 6 can obtain similar performance as that for the GI length of 12 for up to 600km transmission. The use of a GI length longer than 12 might slightly improve the performance, but would reduce the net transmission rate, and an appropriate balance is required in practice.

Previous results are based on the use of all data sub-carriers as pilot tones and 20 training symbols. In practice, it is desirable to use as few as pilot tones per F-OFDM symbol and minimized training symbols. This is of particular value for future packet switched optical networks and applications where the CD values may change frequently such that pilot tones are inserted in the payload symbols to track channel changes instantly. We investigate the system performance as a function of the number of pilot tones, as shown in Fig. 6. 20 symbols are used for training and the number of pilot tones is varied. Similar to the GI length, the required number of pilot tones increases with the transmission distance. The figure shows that four and six pilot tones can achieve near-optimal performance for 600km and 840km respectively. Fig. 7 shows BER versus the number of training symbols for the two channel estimation methods as described in Section II. The figure shows that using six sub-carriers as pilot tones with subsequent frequency-domain interpolation, whilst significantly reducing the overhead, could achieve similar performance as full channel estimation for large training symbol numbers. Furthermore, this method exhibits negligible and moderate penalties for 600km and 840km respectively even when only one symbol is used for training. This makes optical F-OFDM a very attractive solution for future packet switched optical networks with fast-varying CD values.

IV. CONCLUSIONS

We have investigated the channel estimation and compensation in a CD-limited 20Gbit/s 4-ASK optical F-OFDM system. It is shown that SE, rather than CP, based GI is required to enable CD compensation using one-tap equalizers. As few as one optical F-OFDM symbol with four and six pilot tones per symbol can achieve near-optimal performance for 600km and 840km respectively. This makes optical F-OFDM a very attractive solution for future packet switched optical networks with fast-varying CD values.

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